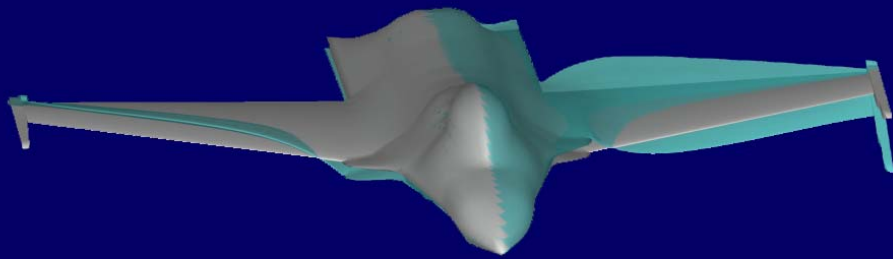


International Workshop on Fluid-Structure Interaction:
Theory, Numerics and Applications - Herrsching, September 29 - October 1, 2008



Transonic Flutter Predictions for a Generic Fighter Configuration

S. Marques, H. Khodaparast,
K. Badcock, J. Mottershead

E C E R T A – Enabling Certification by Analysis



UNIVERSITY OF
LIVERPOOL



Marie Curie
Excellence Team



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CONTENTS

- Motivation
- Schur Complement Method
- Test Cases Description
 - Goland Wing
 - Generic Fighter Configuration
 - Aerodynamics Updating
 - Structural Updating
- Results
- Conclusions



MOTIVATION



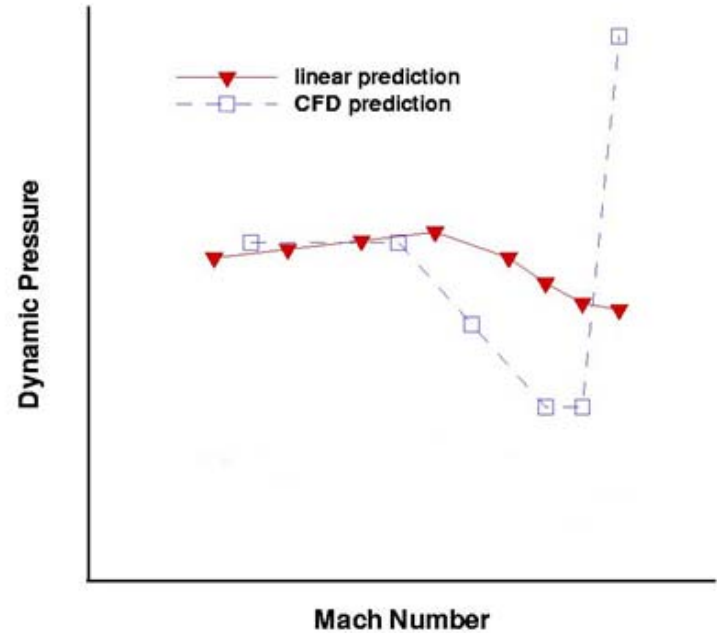
F-16 LCO



MOTIVATION



F-16 LCO



Transonic Flutter Boundary



SCHUR METHOD

- The coupled CFD-CSD system can be described as:

$$\frac{d\mathbf{w}}{dt} = \mathbf{R}(\mathbf{w}, \mu)$$



SCHUR METHOD

- The coupled CFD-CSD system can be described as:

$$\frac{d\mathbf{w}}{dt} = \mathbf{R}(\mathbf{w}, \mu)$$

$$\mathbf{w} = [\mathbf{w}_f, \mathbf{w}_s]^T;$$

$$\mathbf{R} = [\mathbf{R}_f, \mathbf{R}_s]^T$$

μ – Bifurcation
Parameter



SCHUR METHOD

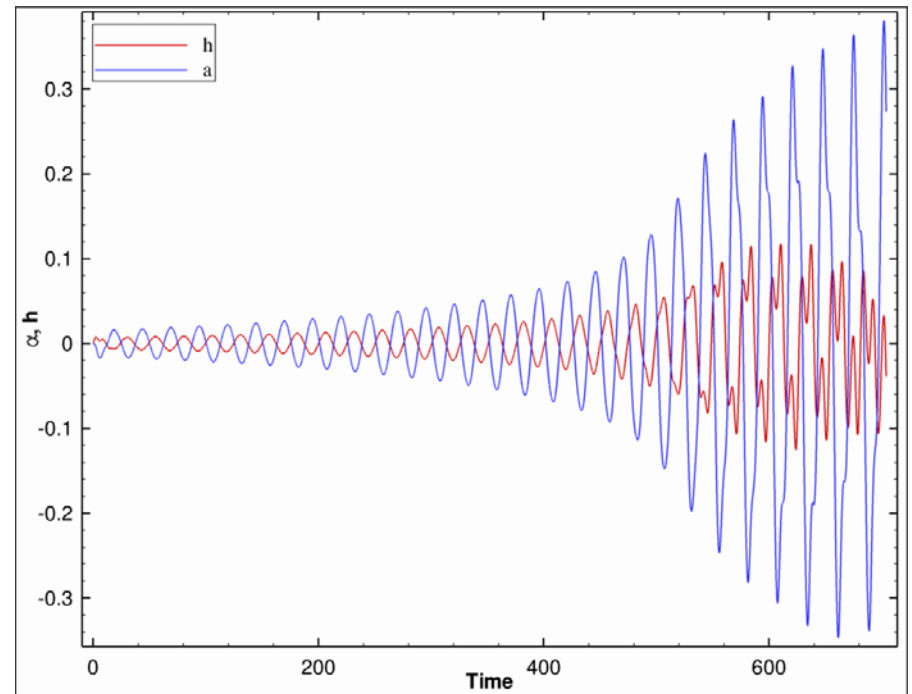
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Parameter



Pitch and Plunge Aerofoil Case

Computationally very intensive
Impractical for flight envelope search



SCHUR METHOD

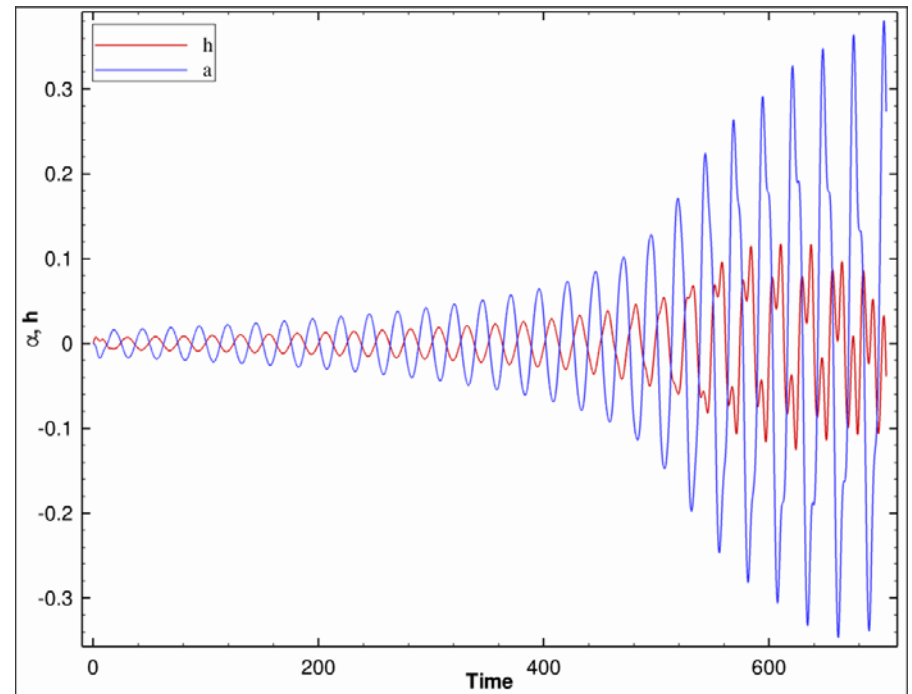
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Parameter



Pitch and Plunge Aerofoil Case

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Impractical for flight envelope search

However...



SCHUR METHOD

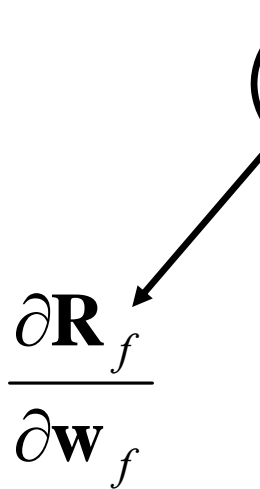
- The eigenvalue problem can be written as:

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$



SCHUR METHOD

- The eigenvalue problem can be written as:

$$\frac{\partial \mathbf{R}_f}{\partial \mathbf{w}_f} \begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$


The diagram shows a circle around the A_{ff} element in the top-left corner of the matrix. An arrow points from this circle to the $\frac{\partial \mathbf{R}_f}{\partial \mathbf{w}_f}$ term on the left side of the equation, indicating that this term is the derivative of the top-left block of the matrix.

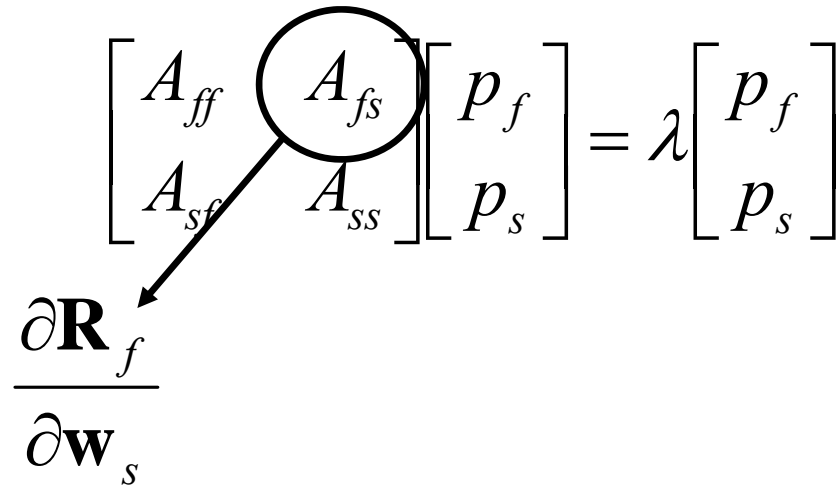


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$\frac{\partial \mathbf{R}_f}{\partial \mathbf{w}_s}$





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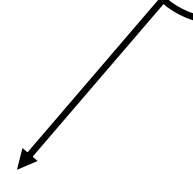
$\frac{\partial \mathbf{R}_s}{\partial \mathbf{w}_f}$



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- Shifted Inverse Power Method

- System becomes ill-conditioned
- Solving in Parallel Difficult

$$z_k = \begin{bmatrix} A_{ff} - \lambda_0 I & A_{fs} \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$$

Badcock et al, AIAA J, 45(6), 1370-1381,2007



SCHUR METHOD

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- Schur Complement formulation:

$$S(\lambda)p_s = \lambda p_s$$

$$S(\lambda) = A_{ss} - A_{sf}(A_{ff} - \lambda I)^{-1}A_{fs}$$

λ is not an eigenvalue of A_{ff}

Bekas and Saad, SIAM Journal of Scientific Computing 27(2) 458, 2005



SCHUR METHOD

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- Schur Complement formulation:

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→ New formulation for
Non-linear Eigenvalue
Problem

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

λ is not an eigenvalue of A_{ff}

Bekas and Saad, SIAM Journal of Scientific Computing 27(2) 458, 2005



SCHUR METHOD

- The new formulation is solved by Newton's Method

$$\frac{\partial \mathbf{F}}{\partial \mathbf{u}} \Delta \mathbf{u} = -\mathbf{F}$$



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$$\begin{bmatrix} S(\lambda) - \lambda I & \frac{\partial S(\lambda)}{\partial \lambda} p_s - p_s \\ q & 0 \end{bmatrix}$$

$$S(\lambda) p_s - \lambda p_s = F$$

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

$$\mathbf{u} = [p_s \ \lambda]^T$$



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Full Evaluation, Expensive



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Full Evaluation, Expensive

$$\mathbf{u} = [p_s \ \lambda]^T$$

But

$$(A_{ff} - \lambda I)^{-1} \approx A_{ff}^{-1} + \lambda A_{ff}^{-1} A_{ff}^{-1} + \lambda^2 A_{ff}^{-1} A_{ff}^{-1} A_{ff}^{-1} + \dots$$



SCHUR METHOD

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But $(A_{ff} - \lambda I)^{-1} \approx A_{ff}^{-1} + \lambda A_{ff}^{-1} A_{ff}^{-1} + \lambda^2 A_{ff}^{-1} A_{ff}^{-1} A_{ff}^{-1} + \dots$

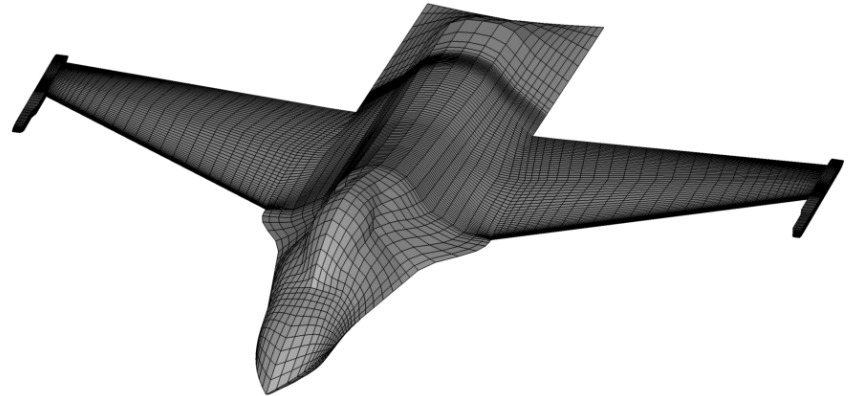
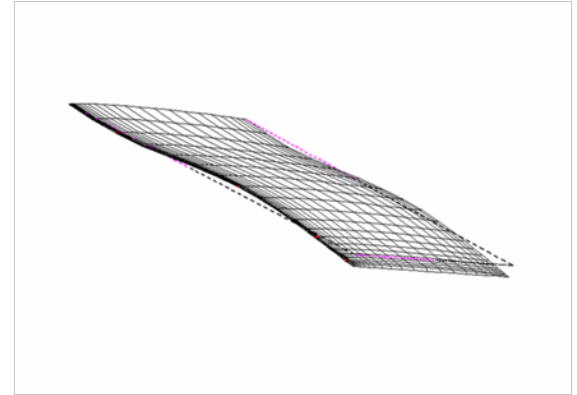
Pre-Compute $A_{sf} A_{ff}^{-1} A_{fs}$ and $A_{sf} A_{ff}^{-2} A_{fs}$

Badcock and Woodgate, AIAA paper 2008-1820, 2008



TEST CASE

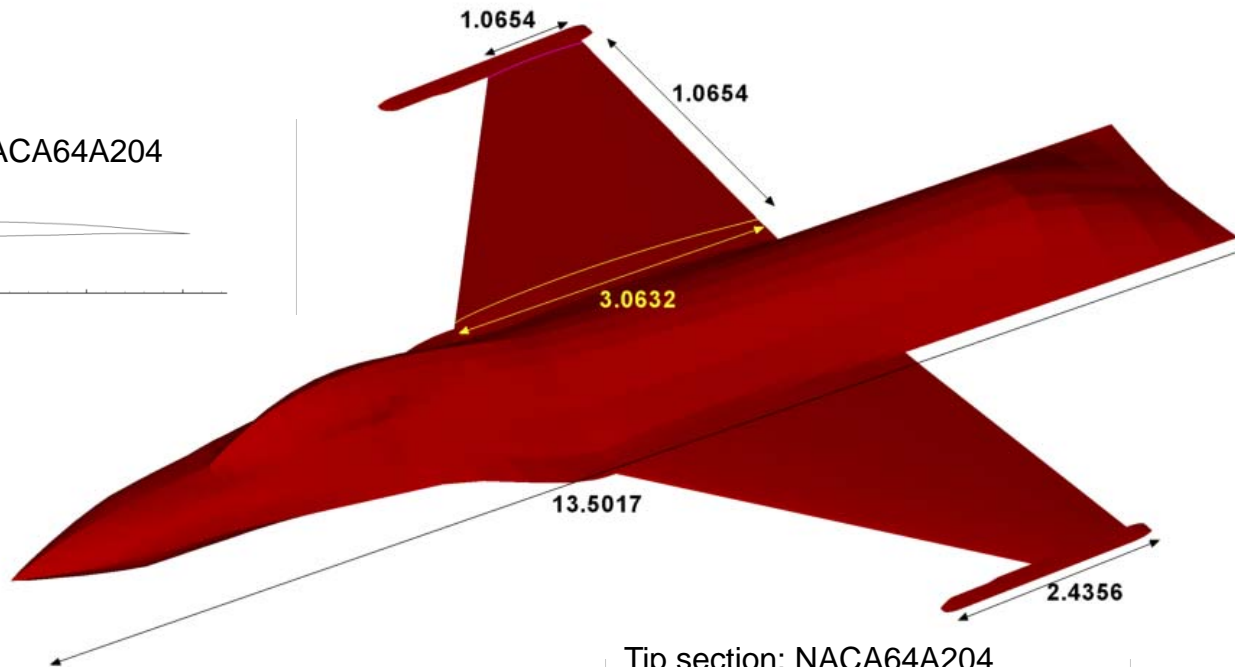
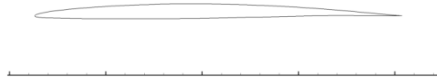
- Two test cases are used to demonstrate the method presented here:
 - Golland Wing
 - Generic Fighter Configuration



TEST CASE

- Aerodynamic updating

Root section: NACA64A204
-1° twist

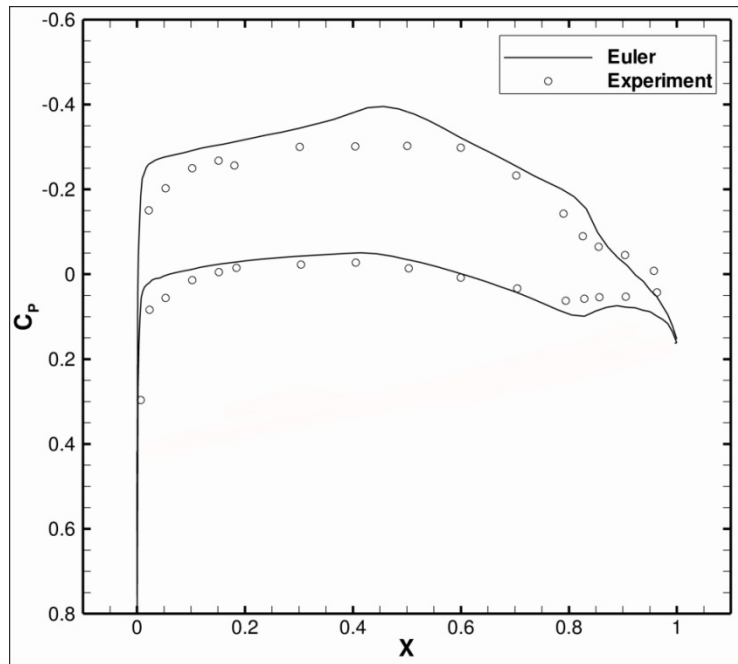


Tip section: NACA64A204
-2.4° twist

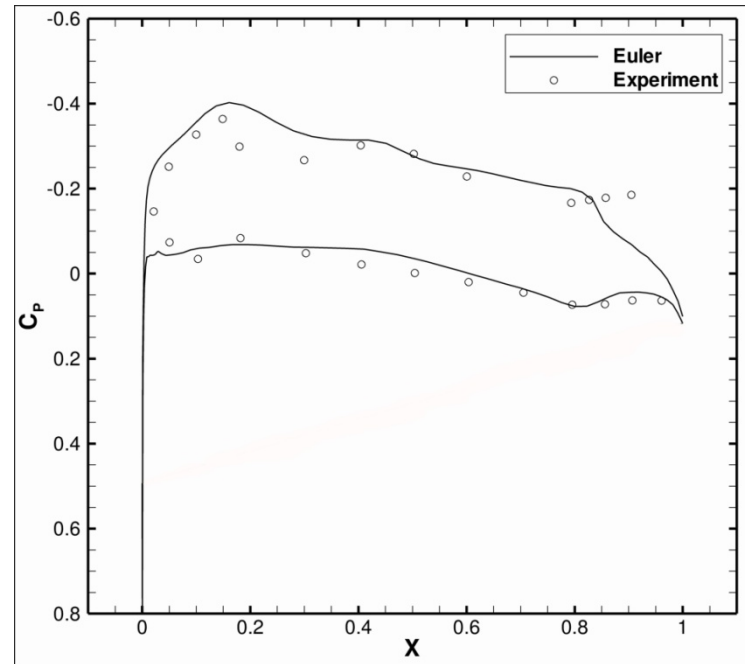


TEST CASE

- Wing aerodynamic configuration was matched to publicly available data



AoA=2.12°; M=0.85; 59% Span



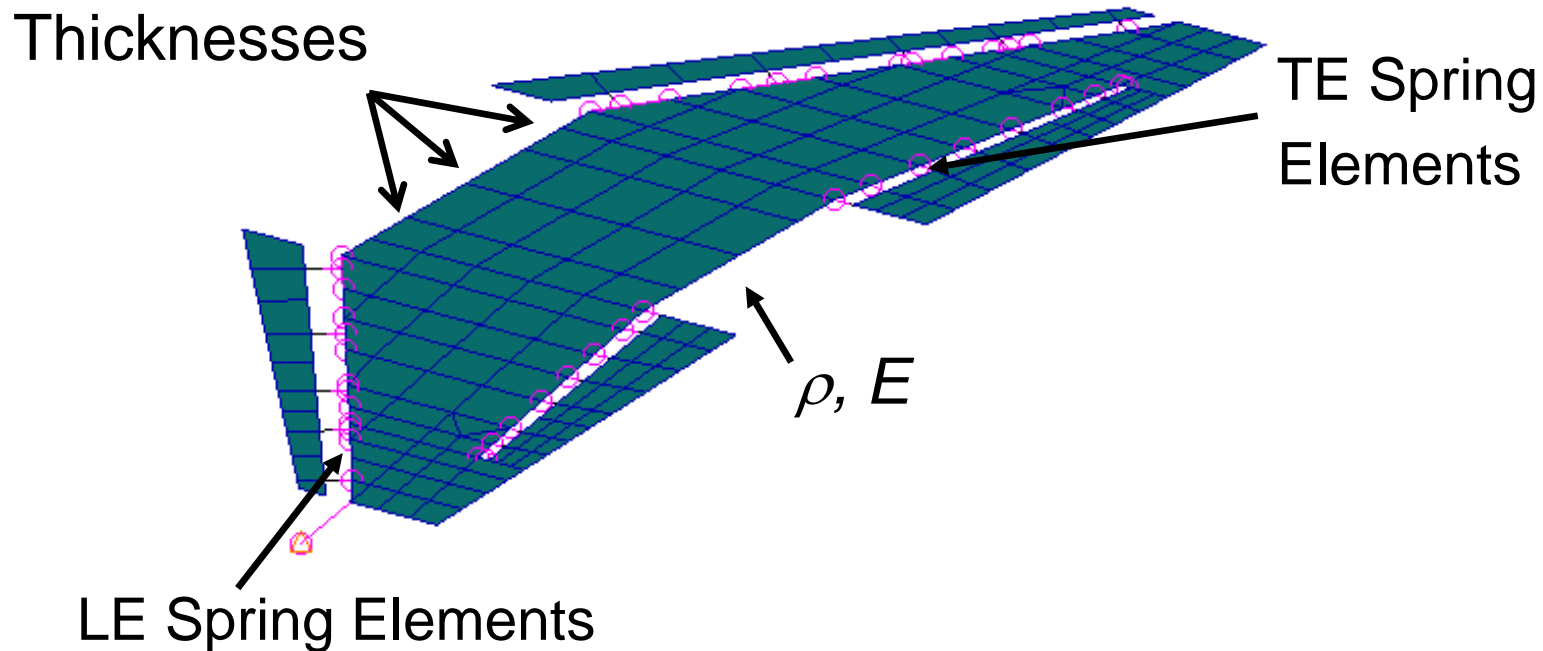
AoA=2.12°; M=0.85; 85% Span

C. Denegri and J. Dubben, IFASD, Munich, 2005



TEST CASE

- FE Model Updating

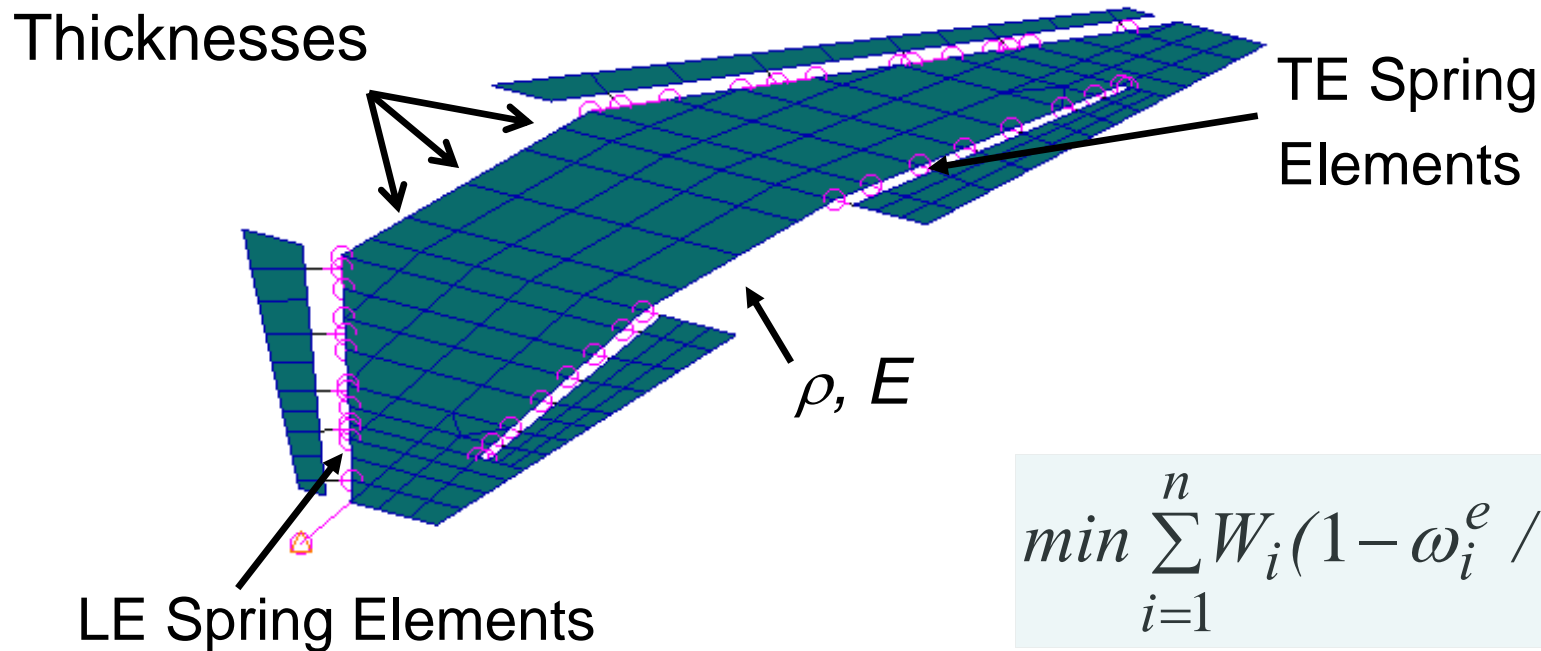


21 Structural Parameters: Directional stiffness, material density, Young modulus, spanwise thickness



TEST CASE

- FE Model Updating



$$\min \sum_{i=1}^n W_i (1 - \omega_i^e / \omega_i^a)^2$$

21 Structural Parameters: Directional stiffness, material density, Young modulus, spanwise thickness



TEST CASE

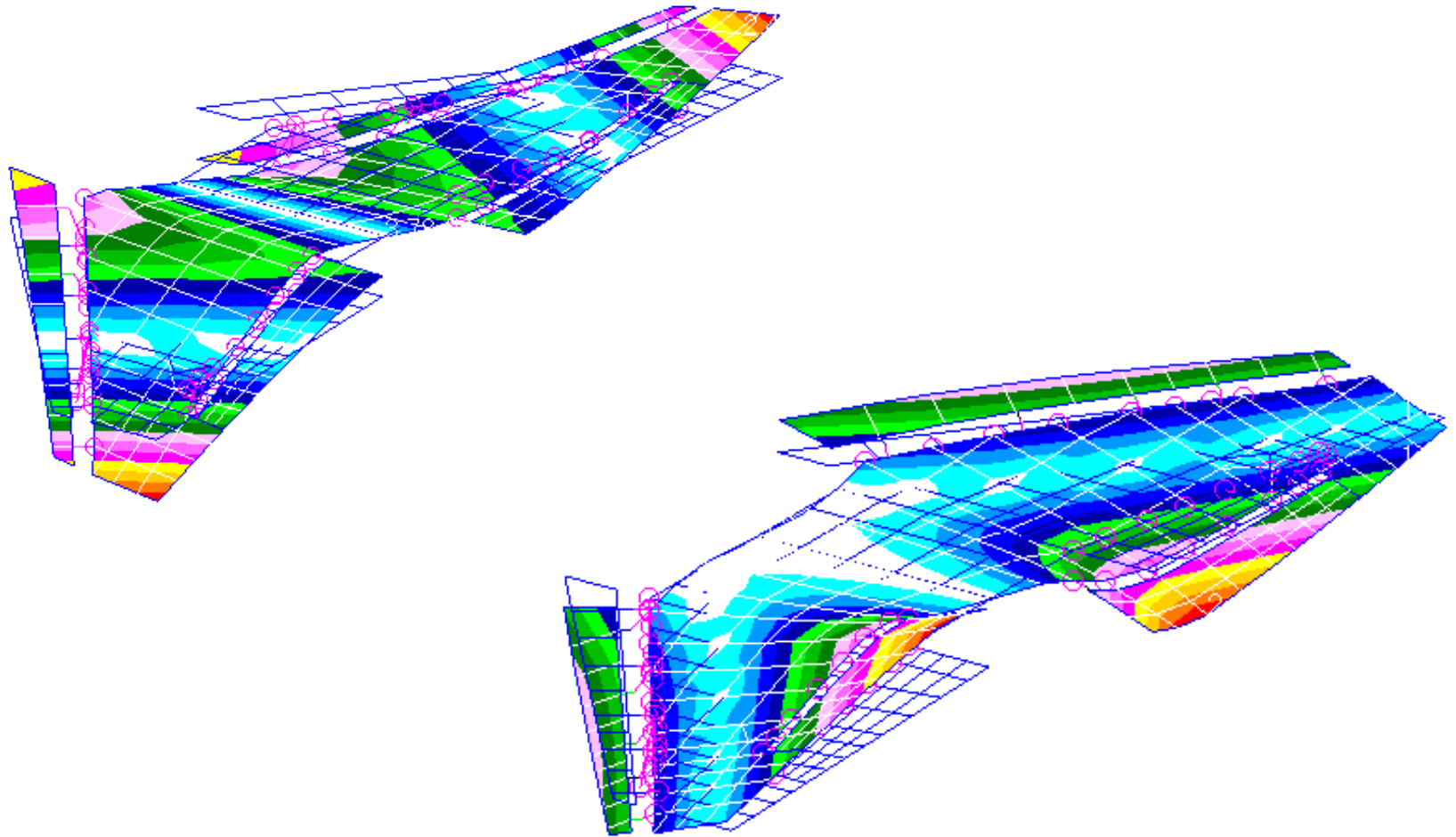
Mode	Initial FE model (Hz)	Denegri data (Hz)	Updated FE model (Hz)	Mode shape
1	7.329		3.920	symmetric
2	11.983	9.191	9.191	antisymmetric
3	17.165	9.964	9.964	antisymmetric
4	21.396		22.452	antisymmetric
5	31.019		22.608	symmetric
6	34.380		24.020	antisymmetric
7	41.109		26.772	symmetric
8	41.217		31.292	antisymmetric
9	44.905		40.040	symmetric
10	45.504		41.695	antisymmetric

C. Denegri, AIAA J. of Aircraft, 37(5), 2000

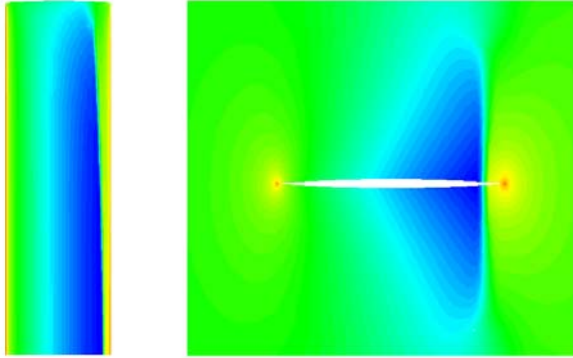


TEST CASE

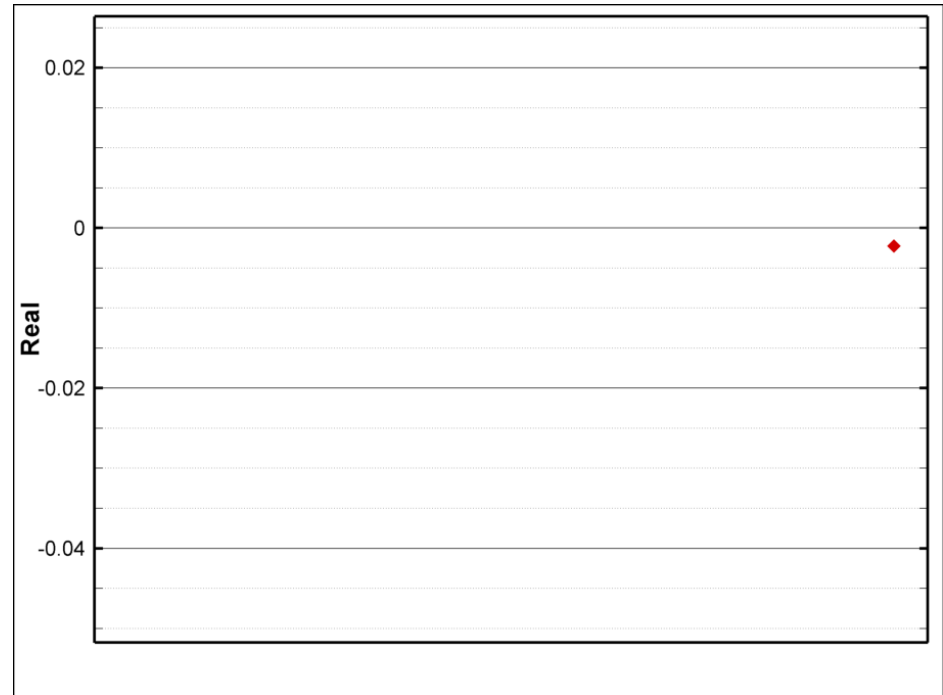
- Updated model mode shapes



GOLAND WING



← Compute Steady State

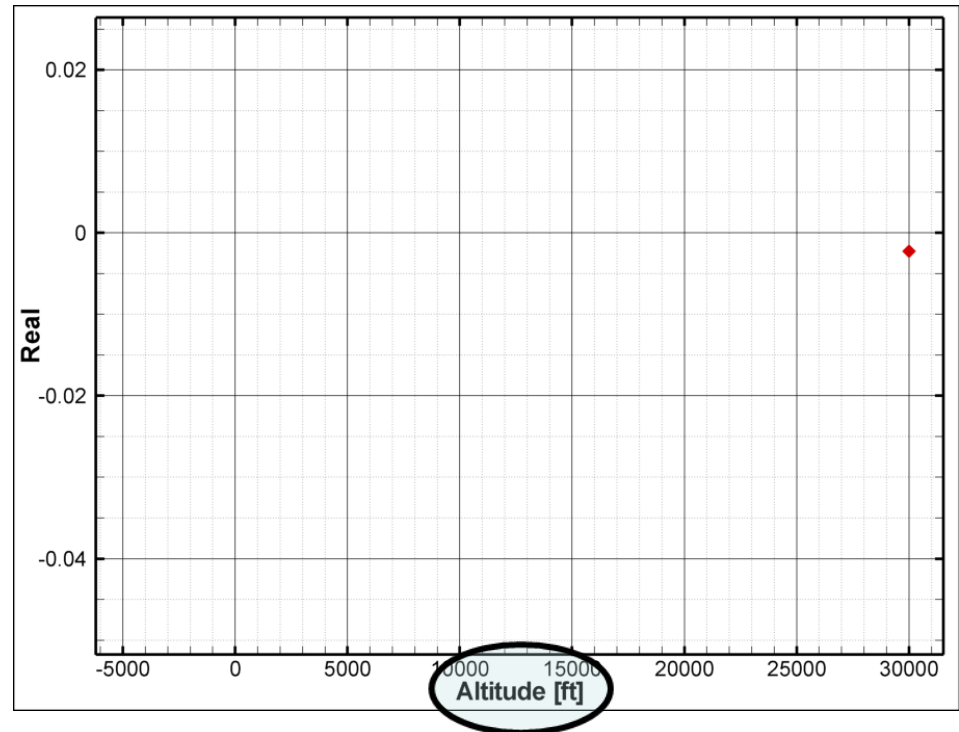
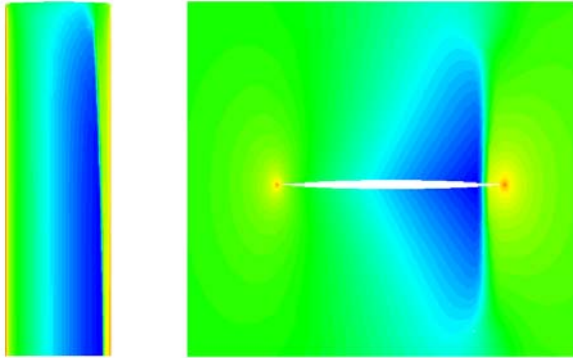


Choose Mode
Pre Compute

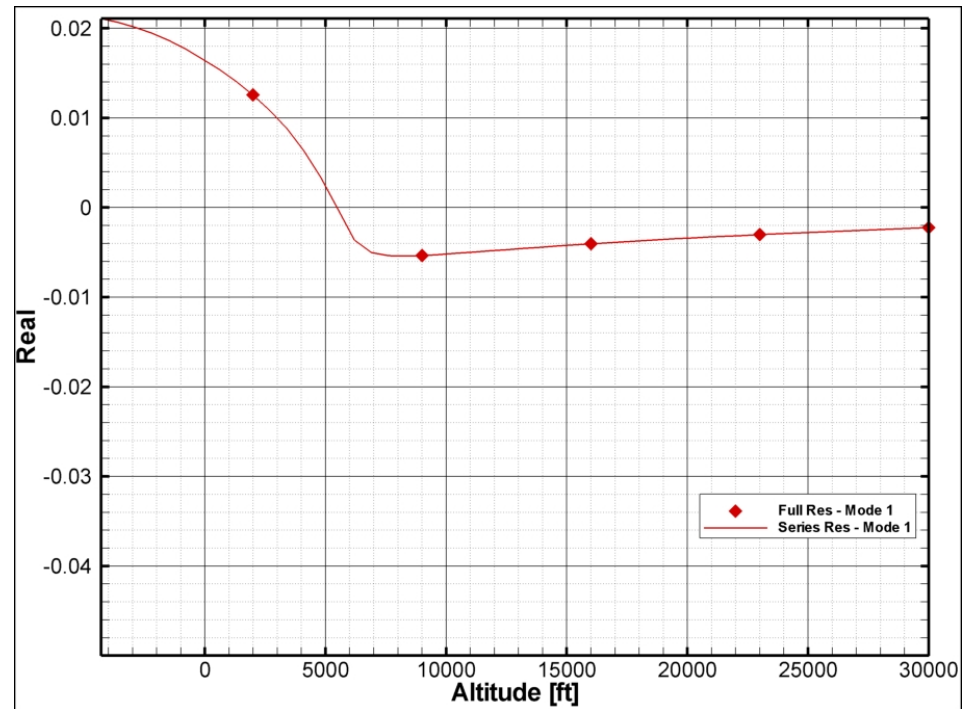
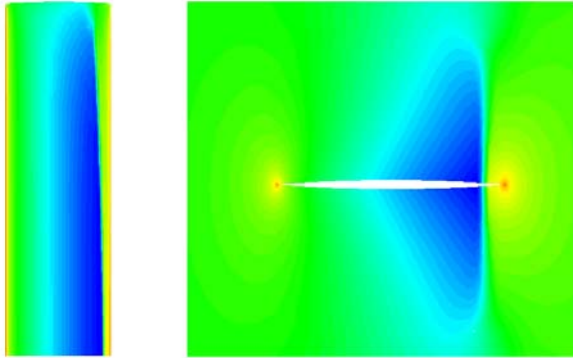
$$A_{sf} A_{ff}^{-1} A_{fs} \text{ and } A_{sf} A_{ff}^{-2} A_{fs}$$



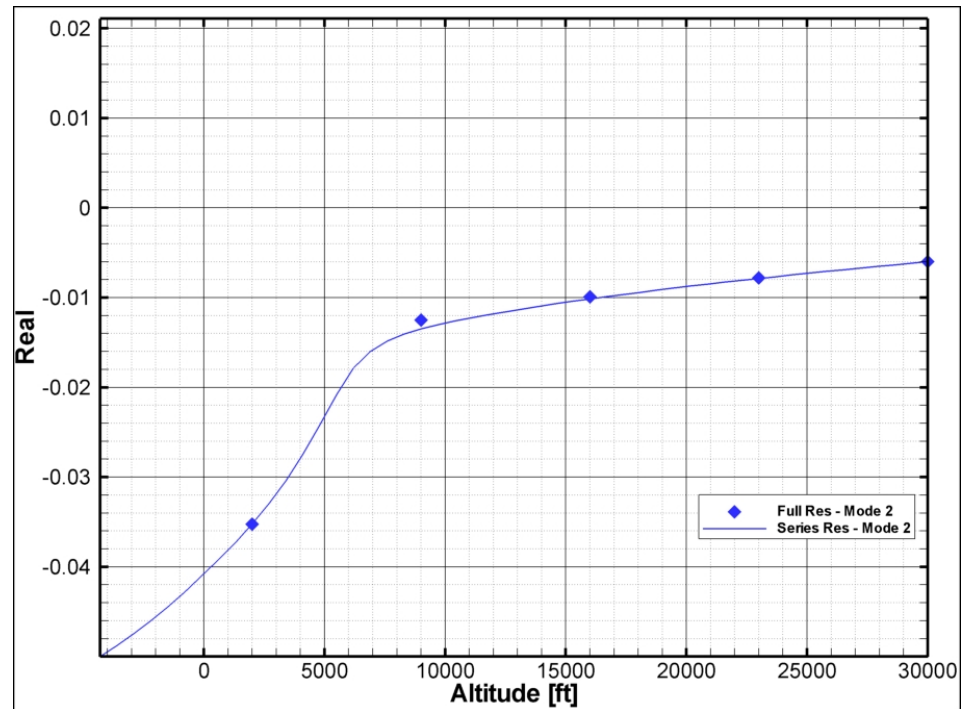
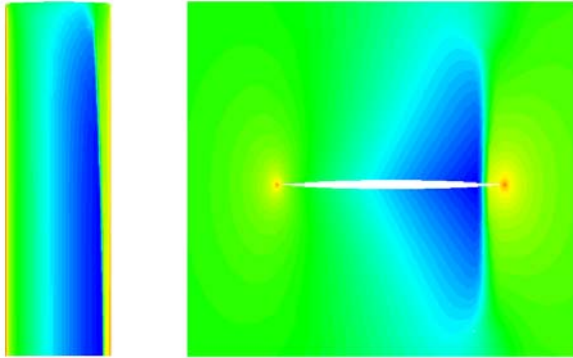
SCHUR METHOD



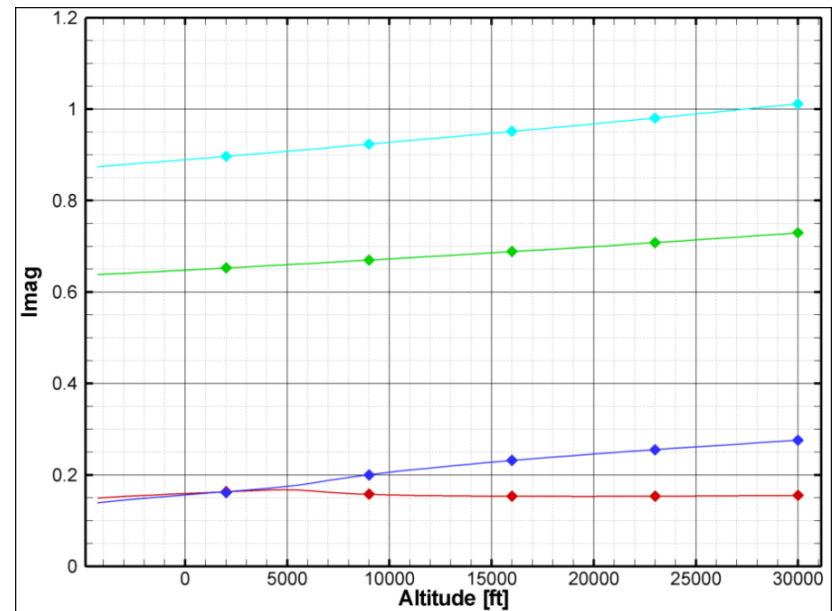
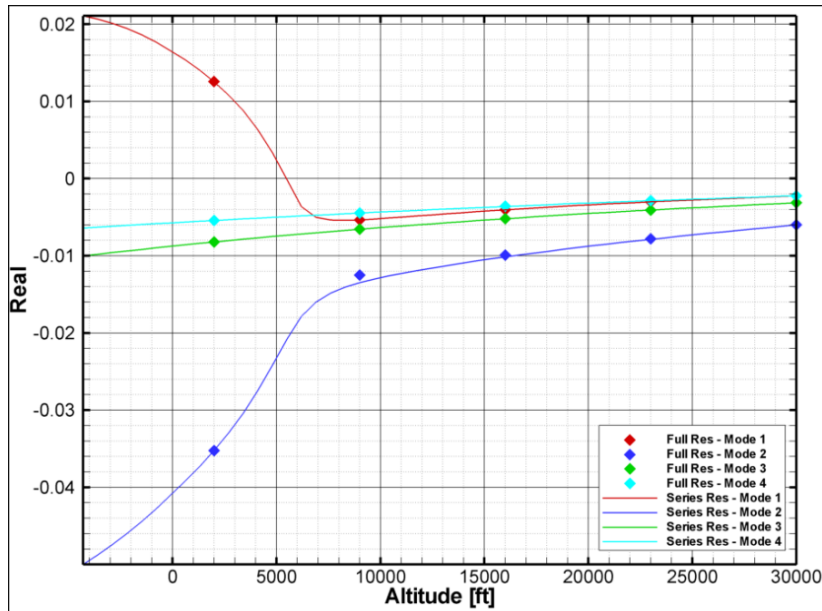
SCHUR METHOD



SCHUR METHOD

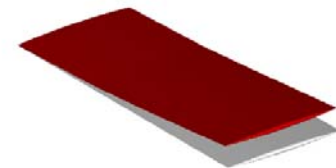


GOLAND WING

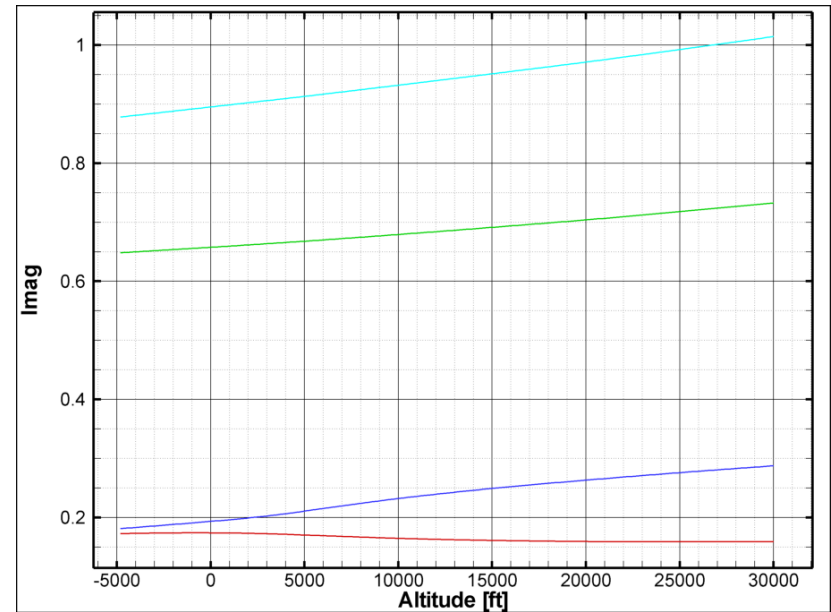
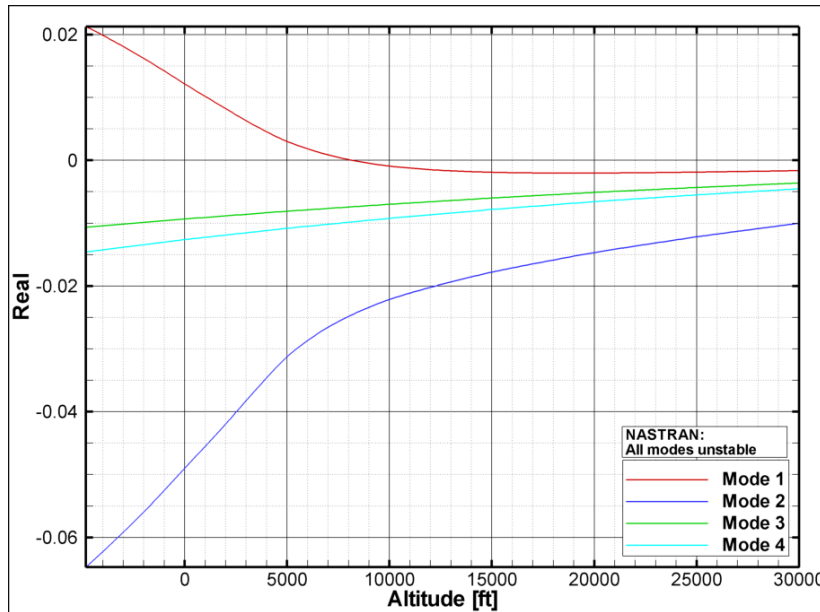


Mach 0.5

- 40k pts grid
- Tracking 4 modes
- 1 Workstation < 12 minutes;
 - Steady State – 1 min
 - $A_{sf} A_{ff}^{-1} A_{fs}$ and $A_{sf} A_{ff}^{-2} A_{fs}$ - 10 min
 - Envelope Sweep < 1min; 5 Full Evaluations- 25 min

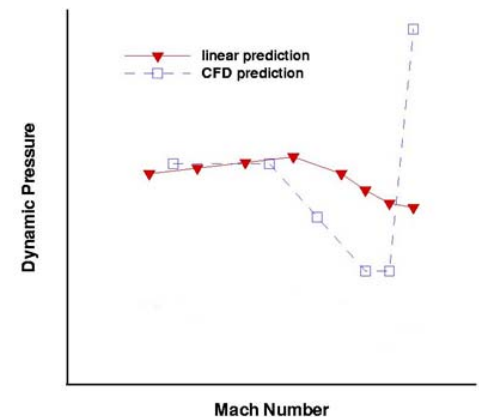


GOLAND WING

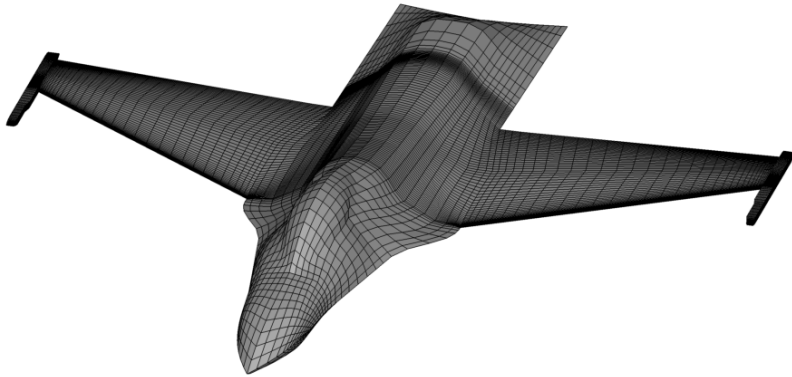


Mach 0.97

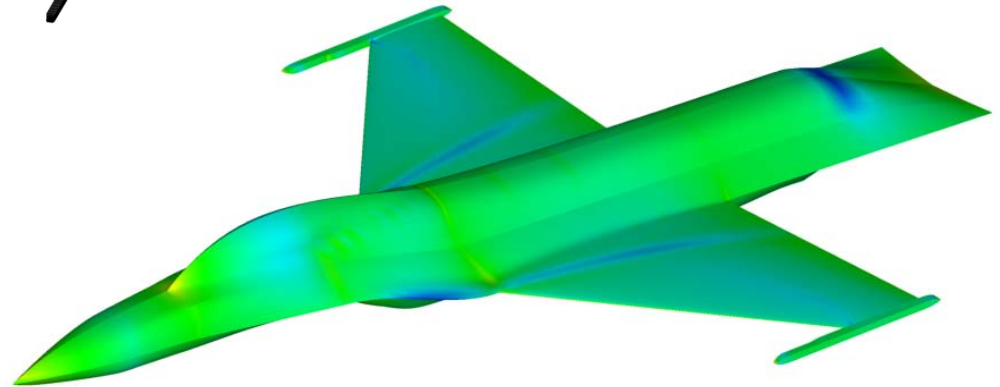
- Coarse grid – 40k pts
- Tracking 4 modes
- 1 Workstation <12 minutes;
 - Steady State – 1 min
 - $A_{sf} A_{ff}^{-1} A_{fs}$ and $A_{sf} A_{ff}^{-2} A_{fs}$ - 10 min
 - Envelope Sweep < 1min



GENERIC FIGHTER



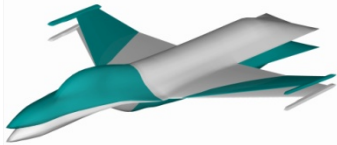
1.1M points



Mach 0.85; AoA 2.12°



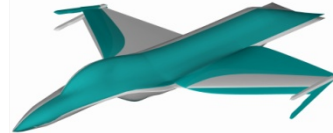
GENERIC FIGHTER



3.920 Hz



9.191 Hz



9.964 Hz



22.452 Hz



22.608 Hz



24.020 Hz



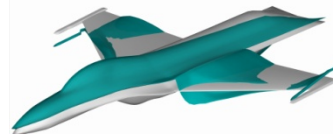
26.772 Hz



31.292 Hz



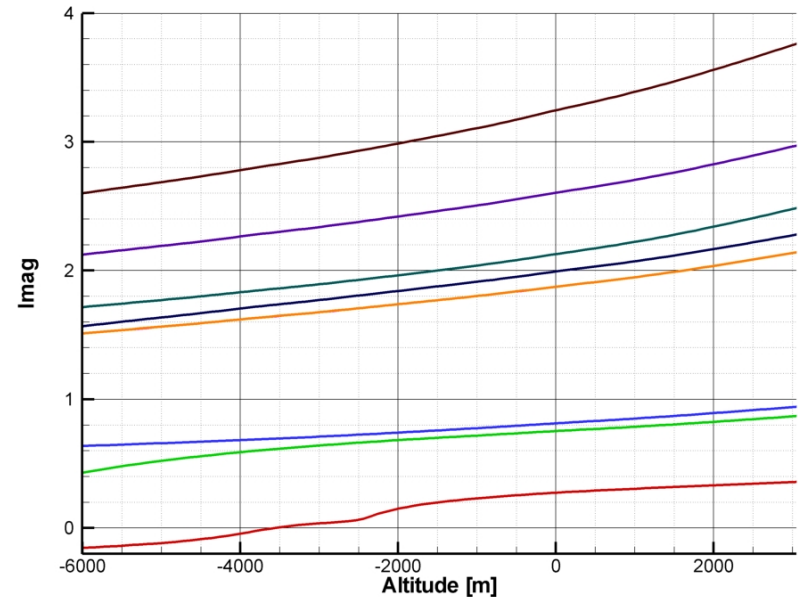
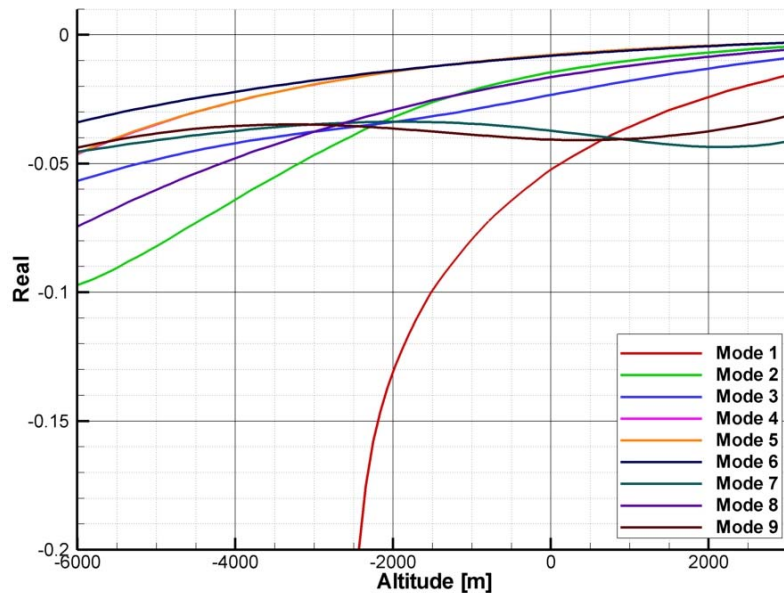
40.04 Hz



41.695 Hz



GENERIC FIGHTER



Mach 0.85; AoA 0°

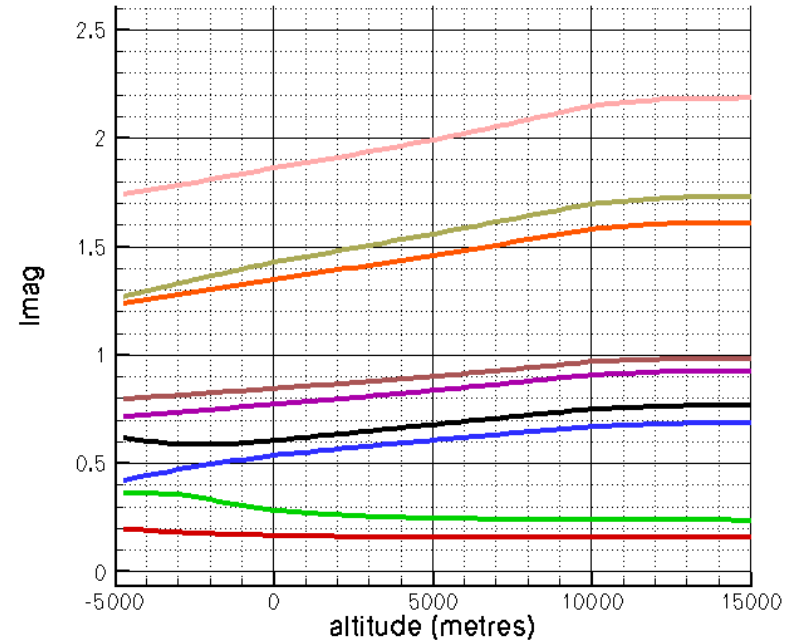
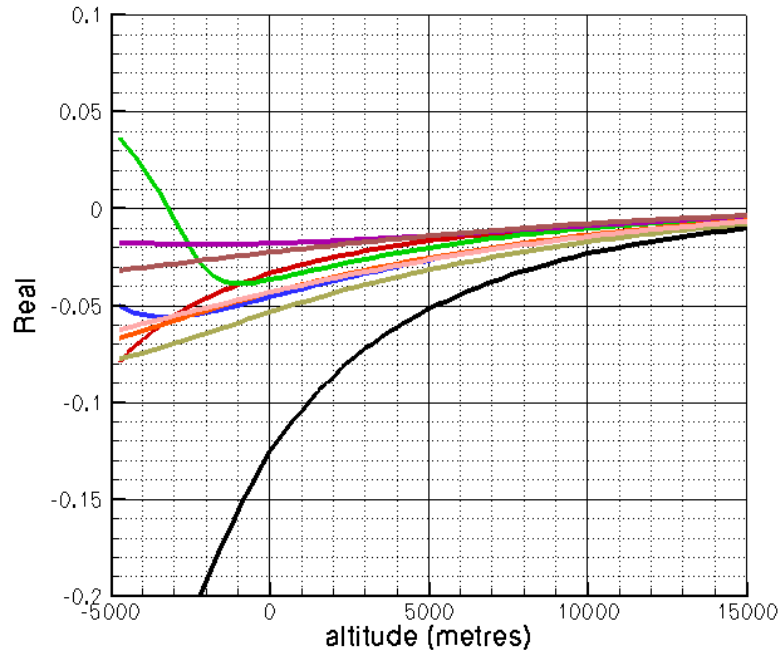
- 32 Processores

- Steady State – 15 min

- $A_{sf} A_{ff}^{-1} A_{fs}$ and $A_{sf} A_{ff}^{-2} A_{fs}$ for 10 Modes - 12 Hours



GENERIC FIGHTER



Mach 0.85; AoA 0°

- 32 Processores
 - Steady State – 15 min
 - $A_{sf} A_{ff}^{-1} A_{fs}$ and $A_{sf} A_{ff}^{-2} A_{fs}$ for 8 Modes - 10 Hours



CONCLUSION

- A very fast method to calculate flutter boundary has been developed
 - The method is easily parallelised
 - It allows for mode tracking at all conditions
 - Series approximation efficient and accurate



CONCLUSION

- A very fast method to calculate flutter boundary has been developed
 - The method is easily parallelised
 - It allows for mode tracking at all conditions
 - Series approximation efficient and accurate
- A realistic test case has been constructed and evaluated
 - Initial FE model improved considerably, to match experimental data
 - Detailed information about mode shapes and interactions obtained



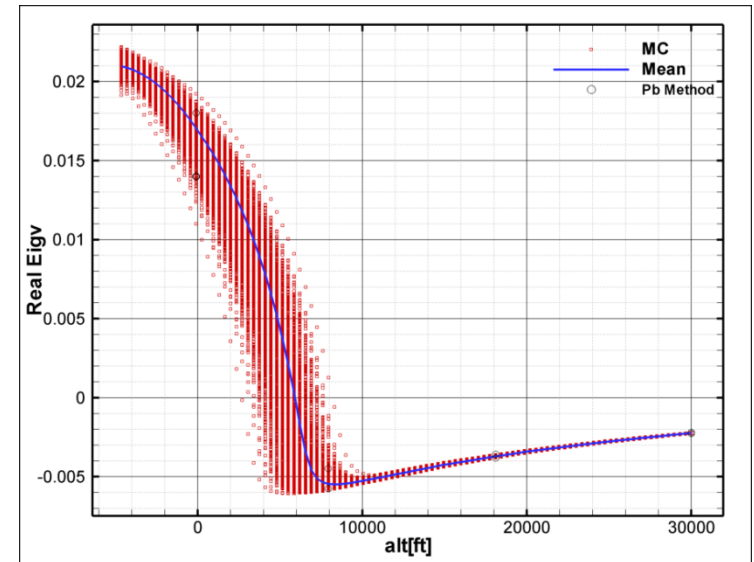
FUTURE WORK

- Expand Generic Fighter Flutter Envelope
- Effects of Structural Uncertainty on Flutter
 - Compare Monte Carlo simulation with Stochastic Methods



FUTURE WORK

- Expand Generic Fighter Flutter Envelope
- Effects of Structural Uncertainty on Flutter
 - Compare Monte Carlo simulation with Stochastic Methods
 - 7 Parameters ▶1000 cases



Q & A

Thank you for your
attention.

Any Questions?

