CFD-BASED SIMULATION AND EXPERIMENT IN HELICOPTER AEROMECHANICS

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Integrating CFD and Experiments in Aerodynamics Glasgow, 8-9 September 2003.



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Helicopter Aeromechanics:

A difficult simulation problem

multiple rotors (with multiple blades) attached to a manoeuvring fuselage

Aerodynamic environment:

- dominated by the rotor wakes
- highly unsteady

Structural dynamics

- large deflections
- aeroelasticity

'Interdisciplinary' effects

- pilot behaviour
- engine dynamic behaviour
- control systems



A highly simplified schematic of the helicopter wake

- strong aerodynamic coupling between well-separated components (e.g main rotor and tail rotor)
- strong coupling between dynamics and aerodynamics

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Wide range of relevant timescales

Fidelity defined in terms of bandwidth over which simulated and real transfer functions agree to within acceptable bounds

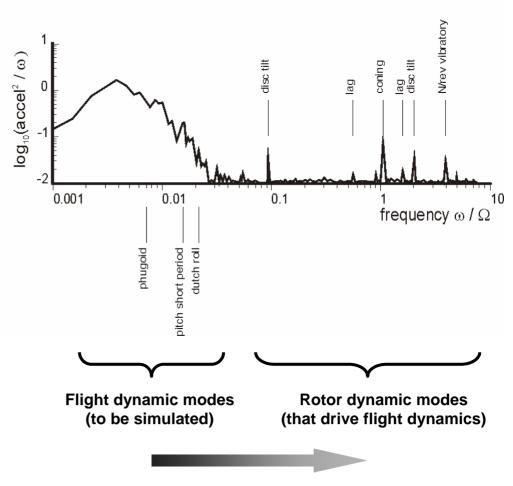
A Rational Approach to Fidelity Enhancement?

Padfield's (1988) hierarchy of models

- Step-by-step approach
- Sequential enhancements to individual constituent physical models

Acceleration Power Spectral Density

(Typical Manoeuvre)



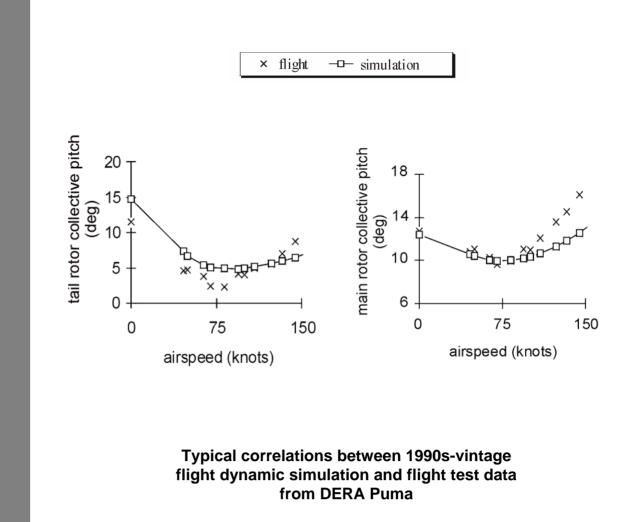
Two orders of magnitude range in timescales

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Typical Simulation Results

- Poor correlation with flight test
- Why?



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An explanation?

- Poor modelling of the wake?
- Simplified dynamic models used to represent delays in development of the inflow through the rotors.

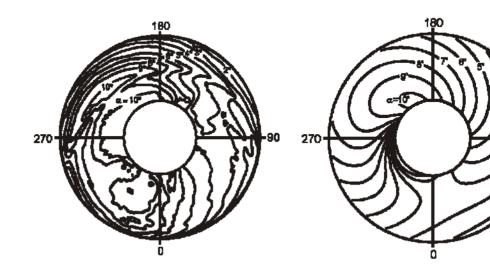
Was 'accepted' within the field that a more realistic representation would be

- 'computationally expensive'

and that

 'small-scale (high frequency) effects not relevant to flight dynamics'

Azimuthal variation of angle of attack experienced by a single rotor blade:



Test data from DERA Puma main rotor Typical 1990s flight dynamic simulation of Puma main rotor

Simulation misses 'real world' flow features such as

- blade-vortex interactions
- tail-rotor interference

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An Examination



Hypothesis: (Houston)

Poor representation of the wake (in terms of its structure and its dynamics) is the reason for poor simulation fidelity.

Approach:

Examine impact of wake fidelity:

- construct a version of Glasgow's RASCAL flight dynamic simulation in which fidelity of wake modelling could be varied:
 - simplified model based on dynamic inflow theory (glorified momentum theory)
 - CFD based model (would be required to incorporate 'real' effects (Brown))
- validate simulations (against flight measured data from DERA Puma.)

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RASCAL Model: Wake Evolution

Simplified model

- represents the delay in the development of the inflow through the rotor.
- dynamically too simple to represent 'real world' effects
- no convection so
- no blade-vortex interactions
- poor representation of manoeuvre-induced effects (e.g. from wake distortion)
- no rotor/rotor interactions

Pitt-Peters Dynamic Inflow Model:

inflow:

 $v(t) = \mathbf{a}(t) \cdot \mathbf{V}$

dynamic equation:

$$[\tau(\mathbf{a}, \dot{\mathbf{x}}_{rotor})]\dot{\mathbf{a}} + \mathbf{a} = [\mathbf{L}(\mathbf{a}, \dot{\mathbf{x}}_{rotor})]\mathbf{F}$$

Typically

 $\mathbf{a} = (a_0, a_{1s}, a_{1c})$

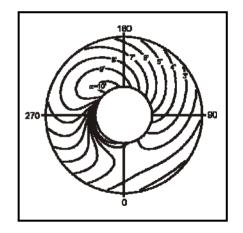
$$v(t) = a_0(t) + a_{1s}(t)\frac{r}{R}\sin\Psi + a_{1c}(t)\frac{r}{R}\cos\Psi$$

representing uniform component as well as longitudinal and lateral gradients of inflow across the rotor disc.



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RASCAL Model: Wake Evolution

CFD-based model

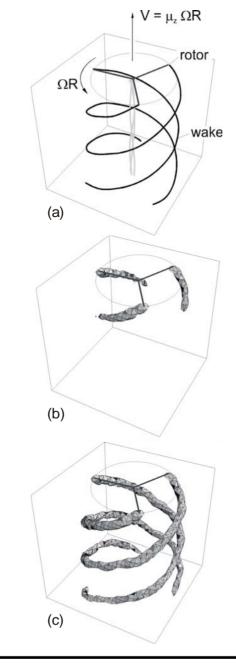
Structured-grid solution of the incompressible, inviscid Vorticity Transport Equation

$$\frac{\partial}{\partial t}\omega + v \cdot \nabla \omega - \omega \cdot \nabla v = S$$
$$\nabla^2 v = -\nabla \times \omega$$

using a variant of the Weighted-Average Flux TVD scheme

together with a lifting-line model for the blade aerodynamics:

$$S = -\frac{\partial}{\partial t}\omega_b + (v_b - v) \cdot \nabla \omega_b$$



Example Physical System:

Rotor in vertical ascent

Highly diffusive behaviour of most conventional CFD-based approaches

Non-diffusive behaviour of vorticity transport approach.

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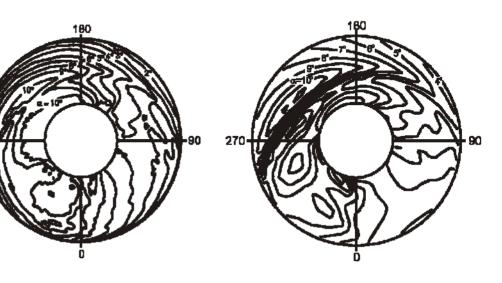


RASCAL Model :

Initial Results:

- Representation of wake effects using the vorticity transport approach looked promising
- What would the impact be on flight dynamic predictions?

Azimuthal variation of angle of attack experienced by a single rotor blade:



Test data from DERA Puma main rotor RASCAL simulation with Vorticity Transport representation of wake

Simulation captures 'real world' flow features such as

- blade-vortex interactions

- tail-rotor interference

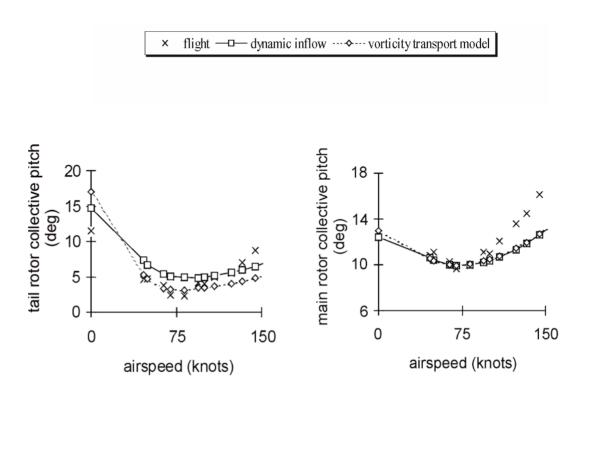
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RASCAL Model :

Flight Dynamic Simulations:

- Disappointing correlation with DERA Puma flight test data.
 - Some improvement where interactions known to dominate (e.g. tail-rotor collective)
 - Many cases where wake model had no effect at all
 - Inconsistent (non-uniform) correlation across speed range
- Explanation?
 - Fuselage drag model?
 - Other physical deficiency?



Typical correlations between RASCAL flight dynamic simulation and flight test data from DERA Puma

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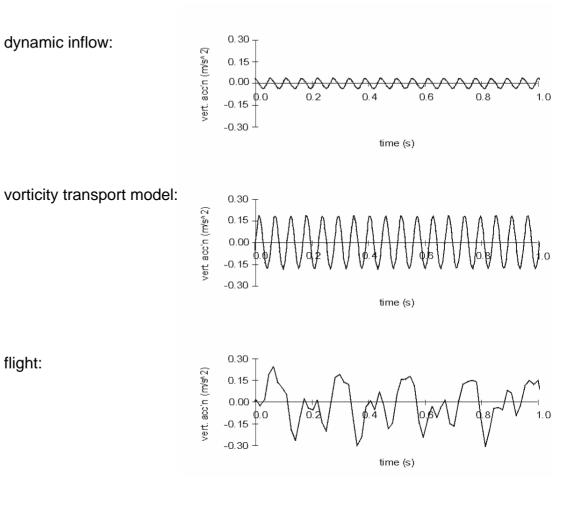
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Validation Issues:

Flight Dynamic Simulations:

- Flight test data too opaque to provide proper environment for validation.
 - Physics too complicated to allow discrimination between possible causes for poor correlation.
 - Unmodelled physical effects? (simulations driven towards maximum complexity)
 - Undocumented defects in system?
 (possible example at right)

Scientifically we are on shaky ground, but there are *engineering* needs.



Correlations between RASCAL flight dynamic simulation of fuselage vibration levels and flight test data from DERA Puma

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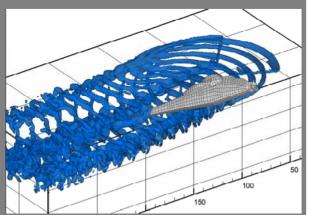
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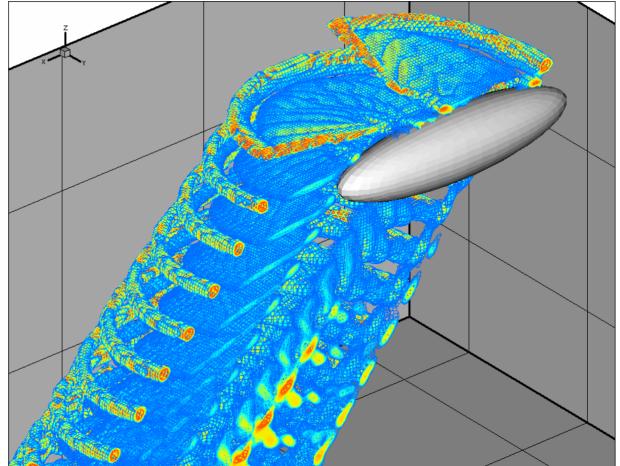


VTM Model :

Essentially the RASCAL model without the flight dynamics

- What happens if we validate this model in a simplified environment?
- laboratory-type experiments on isolated rotors
- physical effects well isolated compared to flight test





Typical VTM simulation: Interaction between a rotor and a simplified fuselage in ascending flight

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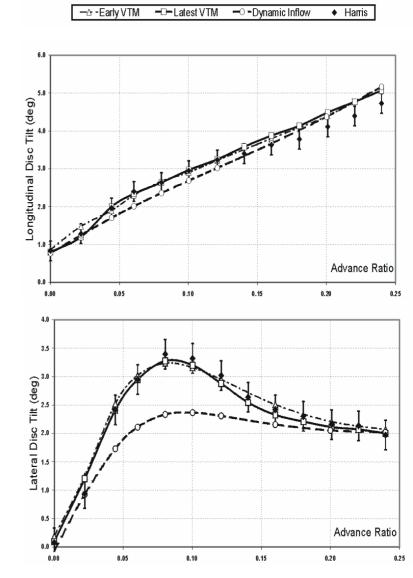
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VTM Model :

Isolated Rotor Performance:

- Harris' 1972 data for rotor flapping as a function of forward speed
- VTM captures distortion of wake downstream of rotor and hence lateral flapping variation.
- Deficiency in blade aero model leads to systematic error in longitudinal flapping variation.
- More subtle contamination by boundary conditions eliminated in latest 'boundary free' VTM.

Good correlation in isolated instance may not imply wider validity of model



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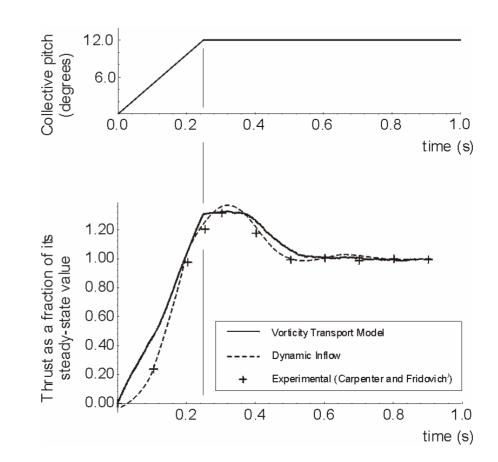
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VTM Model :

Rotor Dynamic Response:

- Carpenter and Fridovich's 1953 data for rotor flapping in response to control input
- Dynamic Inflow model 'designed' around this data
- 'Odd' qualitative features of VTM seen in other models too!
- Curious phenomenon of 'accepted' explanation
 - blade torsion
 - no explicit data to support this
- Example where experimental data has been taken out of context

Experiments must be designed specifically to disprove theory (or simulation)



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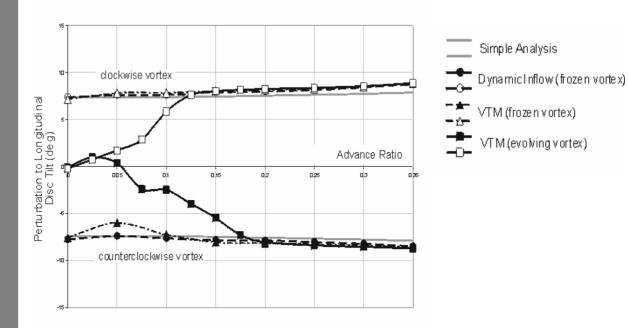
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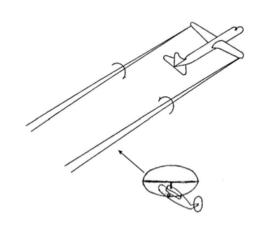
Validation Issues:

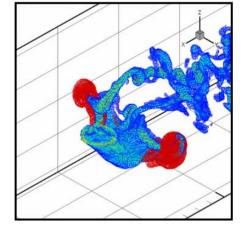
Extrapolation of Validity:

- Good correlation on simplified systems does not translate automatically to valid simulation of more complex systems (e.g. flight test)
- Example at right shows that validity does not even translate between systems with similar complexity if physics is missing
- elimination of 'frozen vortex' assumption changes character of predictions

Can observations be condensed into a global understanding of the validation process?







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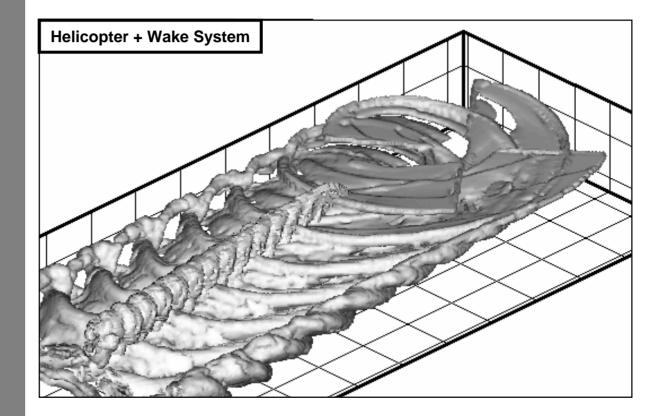
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Conclusions:

Is the behaviour of the wake a paradigm for the behaviour of the whole system?

- Interactions become more important as system complexity is increased
- Interactions introduce couplings that cannot be handled by separable physical models

(hence little hope of incremental fidelity enhancement when simulating a system that is initially too complex)



The challenge for modellers and experimentalists will be to cooperate in designing a range of test cases that bridge the gap between laboratory and flight test, allowing the interactions within the system to be exposed sequentially, then to be captured within simulations.

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