

### **How to Validate Stochastic Finite Element Models from Uncertain Experimental Modal Data**





Slide 1ECERTA Workshop > Yves Govers > 13.-15.09.2010

### **Outline/ Motivation**

- Validation of Finite Element Models on basis of modal data(eigenfrequencies and mode shapes) determined from Modal Survey Test or Ground Vibration Test (GVT)
- Use of gradient based Computational Model Updating Procedures
- $\triangleright$  State of the art: deterministic approach (a single experimentally determined set of modal data is used to identify a deterministic Finite Element Model)
- Goal: probabilistic approach

(use multiple experimentally determined test data sets to identify a Finite Element Model with stochastic parameters)



### **Motivation**

Modal Data Uncertainty

- DLR laboratory benchmark structure **AIR**craft **MOD**el (GARTEUR SM-AG19 replica)
- Made of aluminium with 6 beam like components connected by bolted  $\overline{\phantom{a}}$ joints  $300 z_{500 z}$





### **Motivation**A Source of Modal Data Uncertainty

#### the uncertainty of joint stiffness parameters are generally unknown  $\overline{\phantom{a}}$



VTP vs. HTP

VTP vs. fuselage

wing vs. fuselage

winglet

### **Repeated Modal Survey Test on AIRMOD**



### **Motivation**

Modal Data Uncertainty – Results of AIRMOD Test Campaign

130 times assembled, disassembled, reassembled and re-tested with  $\overline{\phantom{a}}$ random excitation and subsequent automated modal parameter estimation



Significant variation on modal parameters!



### **Introduction** Frequency Clouds

- a number of n tests has been performed
- $\rightarrow$  n frequency pairs  $(f_{11,1},f_{12,1}), (f_{11,2},f_{12,2}),...$  $(f_{11,n},f_{12,n})$  can be plotted
- a scatter diagram  $\overline{\phantom{a}}$ makes the correlation between two frequencies visible





## Frequency Clouds

- The mean values and the standarddeviation  $\,\sigma_{\text{11}}$  and **Introduction**<br>Frequency Clo<br>The mean values<br>and the standard<br>deviation  $\sigma_{11}$  and The mean values and the standard<br>deviation  $\,\sigma_{11}$  and  $\,\sigma$ <br>In case of correlated
- **7** In case of correlated frequency pairs the direction of the frequency cloud is important





### **Introduction** Frequency Clouds

The so calledcovariance ellipse is <sup>a</sup> contour line of equal probability

 $\overline{\phantom{a}}$ Here: 1 x σ





### **Introduction** Frequency Clouds

The so calledcovariance ellipse is <sup>a</sup> contour line of equal probability

Here: 2 x σ 7





### **Introduction** Frequency Clouds

The so calledcovariance ellipse is <sup>a</sup> contour line of equal probability

 $\overline{\phantom{a}}$ Here: 3 x σ





### **Introduction**Frequency Clouds

- the orientation of the ellipse can be visualised by the principal axes
- $\overline{\phantom{1}}$  It shows if the two frequencies are positively or negatively correlated





### **Introduction** Frequency Clouds - Test Data



- $\rightarrow$  Uncertain experimental modal data by **multiple** tests on nominal identical structures
- $\rightarrow$  Uncertainty and correlation of modal data becomes visible if twofrequencies are plotted against each other

### **Test Uncertainty**







# **Introduction**Frequency Clouds - Analysis Data **Mode 13**

- $\rightarrow$  Uncertain analysis modal data by **randomising** a number of **design parameters**
- here: **Monte Carlo Simulation** is utilised in combination with **Latin Hypercube Sampling**







in der Helmholtz-Gemeinschaft

ECERTA Workshop > Yves Govers > 13.-15.09.2010



ECERTA Workshop > Yves Govers > 13.-15.09.2010

### **Stochastic Model Updating** Mean Parameter Adjustment

the difference between mean **<sup>a</sup>**nalytical and **m**easured values can be assembled in a weighted residual vector

$$
\{\bar{\varepsilon}_w\} = [W_v](\{\bar{v}_m\} - \{\bar{v}_a(p)\})
$$

the vector of analytical values  $\{\nu^{}_{a}\}$  can be described by a linearized Taylor series where  $\left[G\right]_i$  represents the sensitivity matrix

$$
\{\bar{v}_a(p)\}_{i+1} = \{\bar{v}_a\}_i + [G]_i \{\Delta \bar{p}\}_i
$$

 $\triangleright$  by minimizing following objective function

 $J = {\bar{\varepsilon}}^T[W_{\varepsilon}]{\bar{\varepsilon}} + {\bar{\Delta p}}^T[W_{p,\varepsilon}]{\bar{\Delta p}} \to \min$ 

a regularization term  $[W_n]$ *i* is used in case of ill-conditioning to improve convergence



### **Stochastic Model Updating** Mean Parameter Adjustment

- $\rightarrow$  the parameter changes are derived using the pseudoinverse of  $[G]$ *i*  $\{\Delta \bar{p}\}_i = [T_{\varepsilon}]_i \{\bar{r}\}_i$ with
- $\triangleright$  where [T] is the transformation matrix  $[T_{\varepsilon}]_i = ([G]^T_i[W_{\varepsilon}][G]_i + [W_{p,\varepsilon}]_i)^{-1}[G]^T_i[W_{\varepsilon}]$



### **Stochastic Model Updating** Covariance Matrix Adjustment

the difference of the covariance matrix of the measured samples and the corresponding analytical covariance matrix can be summarized in a residual matrix

 $[S_{\Delta}]_i = [S_{v_m}] - [S_{v_a(p)}]_i$ 

 $\triangleright$  the analytical covariance matrix can derived from the Taylor series expansion of the analytical vector under the  $\texttt{assumption}$  of  $\{v_a\}$  and  $\{\Delta p\}$ to be uncorrelated at iteration step i

$$
[S_{v_a(p)}]_{i+1} = \left[ \mathbf{Cov} \left( \{v_a\}_i + [G]_i \{\Delta p\}_i, \{v_a\}_i + [G]_i \{\Delta p\}_i \right) \right]
$$
  
= 
$$
[S_{v_a}]_i + [G]_i [S_{\Delta p}]_i [G]_i^T
$$



### **Stochastic Model Updating** Covariance Matrix Adjustment

by minimizing following objective function with the Frobenius Norm of the residual matrix  $\ [S_{\Delta}]$ 

$$
J_S = \frac{1}{2} ||[W_S][S_\Delta][W_S]^T||_F^2 \to \min
$$

- $\triangleright$  the parameter covariance matrix changes (increments) are derived from with
- and the transformation matrix [ $T^{}_{\Sigma}$ ]

 $[T_{\Sigma}]_i = ([G]^T_i[W_{\Sigma}][G]_i + [W_{p,\Sigma}]_i)^{-1} [G]^T_i[W_{\Sigma}]$ 



### **Test Case – AIRMOD**  Rigid Body Modes





### **Test Case – AIRMOD**  Rigid Body Modes



### **Test Case – AIRMOD rigid body modes**

Initial Frequency Deviations



**Deutsches Zentrum** für Luft- und Raumfahrt e.V. in der Helmholtz-Gemeinschaft

ECERTA Workshop > Yves Govers > 13.-15.09.2010 Slide 22

### **Test Case – AIRMOD rigid body modes** Updated Frequency Deviations iteration step 12 analysis experiment  $0,2$  $0.3$  $[0,6]$ <u>0.</u>7  $0.8$  $\mathbf{0.9}$ **Deutsches Zentrum**



für Luft- und Raumfahrt e.V. in der Helmholtz-Gemeinschaft

ECERTA Workshop > Yves Govers > 13.-15.09.2010 Slide 23

### **Test Case – AIRMOD rigid body modes**

### **Convergence**

in der Helmholtz-Gemeinschaft



ECERTA Workshop > Yves Govers > 13.-15.09.2010

### **Conclusions and Outlook**

- Conventional model updating procedure has been extended by an equation adjusting the model parameter covariances
- $\triangleright$  Developed algorithm was applied to the rigid body modes of an aircraft like laboratory structure AIRMOD
- $\triangleright$  Test case shows a good convergence
- $\triangleright$  Frequency clouds match well: adjusted parameters represent the uncertainty of the measurement data
- $\triangleright$  In a second step the elastic modes will be updated





### **Thank you for your attention!**

### **Yves Govers, German Aerospace Center (DLR)**



Slide 26ECERTA Workshop > Yves Govers > 13.-15.09.2010