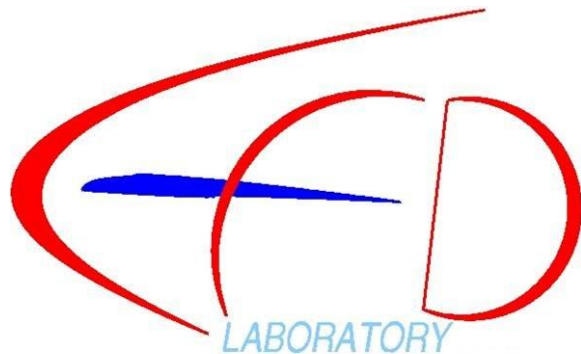




Prediction of Bifurcation Onset of Large Order Aeroelastic Models



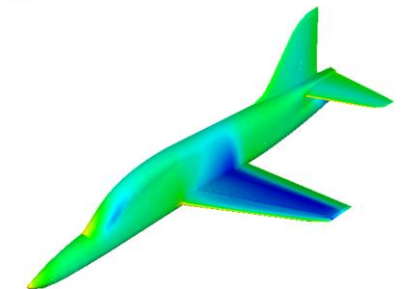
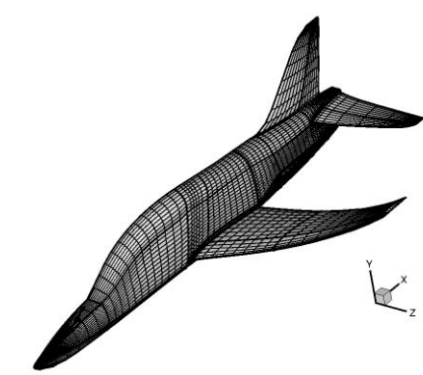
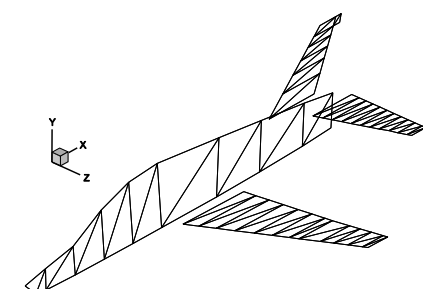
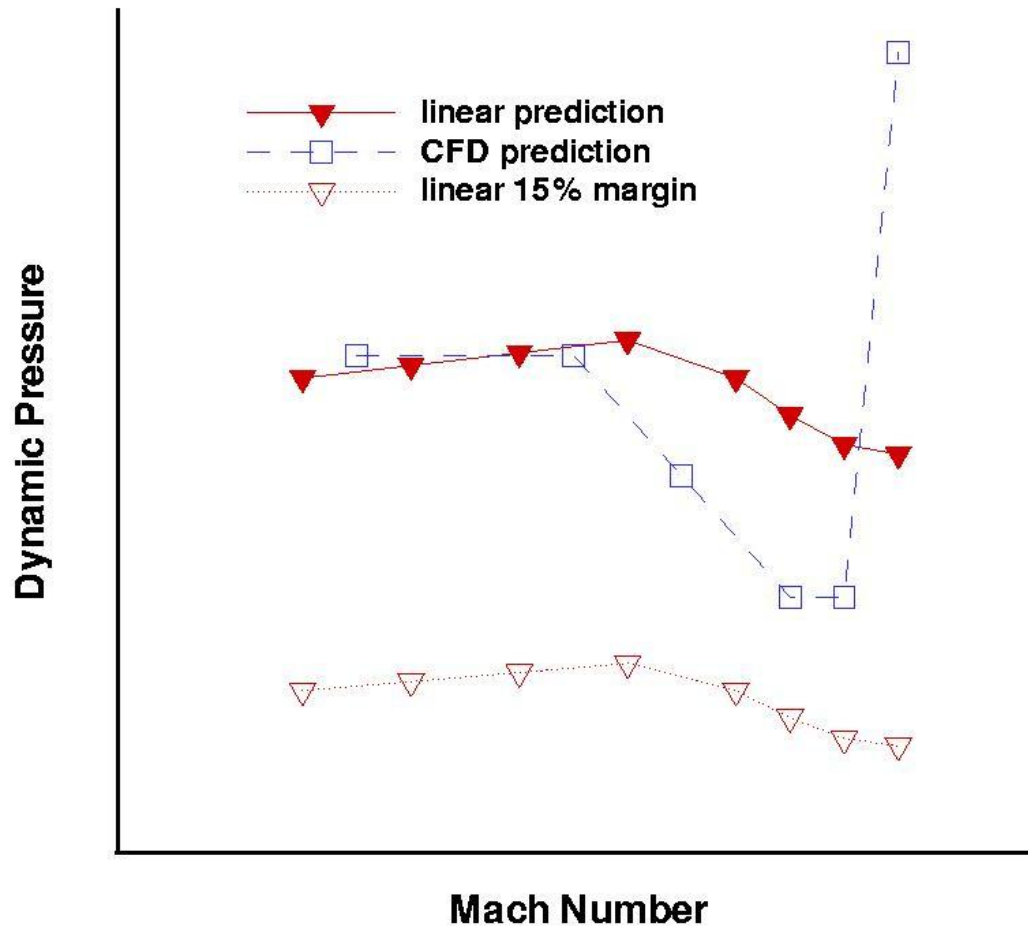
K.J.Badcock and M.A. Woodgate
CFD Laboratory,
University of Liverpool,
UK

www.cfd4aircraft.com



Marie Curie Excellence Team
Enabling Certification by Analysis





Woodgate, M. Badcock, K.J. Rampurawala, A.M. Richards, B.E. Nardini D. and Henshaw M. Aeroelastic calculations for the Hawk aircraft using the Euler equations, **Journal of Aircraft**, 42(4), 2005, 1005-1012.

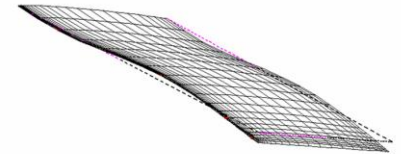
Denley, C.J., Eccles, T.A., Cross, A.G.T., Practical Unsteady CFD Application to Aircraft Flutter and Limit Cycle Oscillation, **RTO-AVT-152**, Loen, May, 2008

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \mathbf{p} = \lambda \mathbf{p}$$

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \mathbf{p} = \lambda \mathbf{p}$$

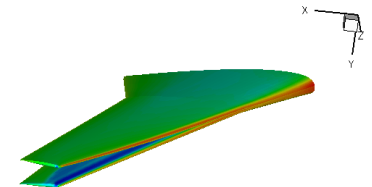
Badcock et al, **J Aircraft**, 42(3), 731-737, 2005

- solved an augmented system for the critical eigenvalue
- Assumptions/Limitations
 - good initial guess at flutter frequency
 - Symmetric problem
 - Sequential calculation



Badcock et al, **AIAA J**, 45(6), 1370-1381, 2007

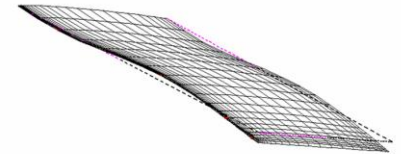
- Aeroelastic eigenvalues using the Inverse Power Method
- Assumptions/Limitations
 - Sequential calculation
 - Mode tracking



$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \mathbf{p} = \lambda \mathbf{p}$$

Badcock et al, **J Aircraft**, 42(3), 731-737, 2005

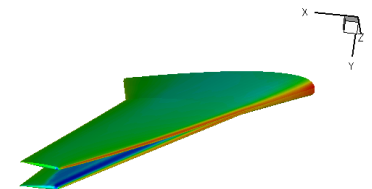
- solved an augmented system for the critical eigenvalue
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 - Sequential calculation



Badcock et al, **AIAA J**, 45(6), 1370-1381, 2007

- Aeroelastic eigenvalues using the Inverse Power Method
- Assumptions/Limitations
 - Sequential calculation
 - Mode tracking

Addressed in
current work



Inverse Power Method

$$z_k = \begin{bmatrix} A_{ff} - \lambda_0 I & A_{fs} \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$$

Inverse Power Method

$$z_k = \begin{bmatrix} A_{ff} - \lambda_0 I & A_{fs} \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$$

The diagram illustrates the Inverse Power Method. It shows the iteration formula $z_k = \begin{bmatrix} A_{ff} - \lambda_0 I & A_{fs} \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$. The eigenvalue λ_0 is circled in both the top-left and bottom-right blocks of the matrix. Two arrows point from these circled λ_0 terms to a red box labeled "shift", indicating that λ_0 is the shift value used in the matrix inversion.

Inverse Power Method

$$z_k = \begin{bmatrix} A_{ff} & -\lambda_0 I \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$$

Diagram illustrating the Inverse Power Method iteration matrix. The matrix is partitioned into four blocks: A_{ff} , A_{sf} , A_{fs} , and A_{ss} . The shift parameter λ_0 is circled in both the top-right and bottom-right blocks, with arrows pointing to a red box labeled "shift".

- good shift needed for convergence
 - Better shift - iteration matrix becomes more singular
- Iterative solvers thrown at solving this problem in parallel
 - good methods available but none has really done the job

Inverse Power Method

$$z_k = \begin{bmatrix} A_{ff} - \lambda_0 I & A_{fs} \\ A_{sf} & A_{ss} - \lambda_0 I \end{bmatrix}^{-1} x_{k-1}$$

New thinking needed

- good shift needed for convergence
 - Better shift - iteration matrix becomes more singular
- Iterative solvers thrown at solving this problem in parallel
 - good methods available but none has really done the job

Eigenvalue Problem

$$\begin{bmatrix} \mathbf{A}_{ff} & \mathbf{A}_{fs} \\ \mathbf{A}_{sf} & \mathbf{A}_{ss} \end{bmatrix} \begin{bmatrix} \mathbf{p}_f \\ \mathbf{p}_s \end{bmatrix} = \lambda \begin{bmatrix} \mathbf{p}_f \\ \mathbf{p}_s \end{bmatrix}$$

Eigenvalue Problem

$$\begin{bmatrix} \mathbf{A}_{ff} & \mathbf{A}_{fs} \\ \mathbf{A}_{sf} & \mathbf{A}_{ss} \end{bmatrix} \begin{bmatrix} \mathbf{p}_f \\ \mathbf{p}_s \end{bmatrix} = \lambda \begin{bmatrix} \mathbf{p}_f \\ \mathbf{p}_s \end{bmatrix}$$

Schur complement version

$$S(\lambda) \mathbf{p}_s = \lambda \mathbf{p}_s$$

(Bekas and Saad, SIAM
Journal of Scientific
Computing 27(2) 458, 2005)

$$S(\lambda) = \mathbf{A}_{ss} - \mathbf{A}_{sf} (\mathbf{A}_{ff} - \lambda \mathbf{I})^{-1} \mathbf{A}_{fs}$$

λ Not an eigenvalue of \mathbf{A}_{ff}

Eigenvalue Problem

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$

Schur complement version

(Bekas and Saad, SIAM
Journal of Scientific
Computing 27(2) 458, 2005)

$$S(\lambda) p_s = \lambda p_s$$

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

λ Not an eigenvalue of A_{ff}

Good! Small order
nonlinear eigenvalue
problem

Eigenvalue Problem

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$

Schur complement version

$$S(\lambda) p_s = \lambda p_s$$

(Bekas and Saad, SIAM
Journal of Scientific
Computing 27(2) 458, 2005)

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

λ Not an eigenvalue of A_{ff}

Good! – solves ill
conditioning problem

Eigenvalue Problem

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$

Schur complement version

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(Bekas and Saad, SIAM
Journal of Scientific
Computing 27(2) 458, 2005)

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

λ Not an eigenvalue of A_{ff}



Bad! – re-evaluate S at every nonlinear step

But

$$(A_{ff} - \lambda I)^{-1} \approx A_{ff}^{-1} + \lambda A_{ff}^{-1} A_{ff}^{-1}$$

Eigenvalue Problem

$$\begin{bmatrix} A_{ff} & A_{fs} \\ A_{sf} & A_{ss} \end{bmatrix} \begin{bmatrix} p_f \\ p_s \end{bmatrix} = \lambda \begin{bmatrix} p_f \\ p_s \end{bmatrix}$$

Schur complement version

$$S(\lambda) p_s = \lambda p_s$$

(Bekas and Saad, SIAM
Journal of Scientific
Computing 27(2) 458, 2005)

$$S(\lambda) = A_{ss} - A_{sf} (A_{ff} - \lambda I)^{-1} A_{fs}$$

λ Not an eigenvalue of A_{ff}

Bad! – re-evaluate S at every nonlinear step

But

$$(A_{ff} - \lambda I)^{-1} \approx A_{ff}^{-1} + \lambda A_{ff}^{-1} A_{ff}^{-1}$$

Pre-compute – valid if λ is small

Method

To track an aeroelastic eigenvalue

1. Choose normal mode frequency as a shift

$$S(\lambda) = (A_{ss} - \lambda_0 I) - A_{sf} (A_{ff} - \lambda I - \lambda_0 I)^{-1} A_{fs}$$

2. Precompute

$$A_{sf} (A_{ff} - \lambda_0 I)^{-1} A_{fs} \quad A_{sf} (A_{ff} - \lambda_0 I)^{-2} A_{fs}$$

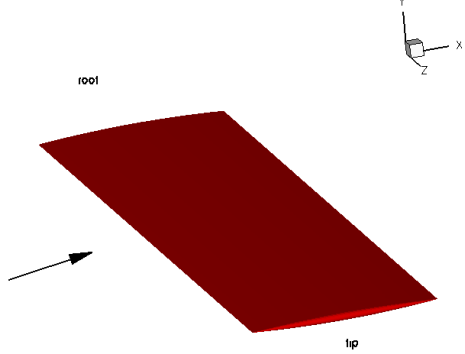
3. Solve nonlinear eigenvalue problem by Newton's method
 - Use **series** approximation to generate function (very cheap)
 - Use **full** evaluation to generate function (more expensive)
 - In both cases use series approximation for LHS
4. Change Altitude and repeat step 3

Comments

- Series expansion to drive convergence
 - Full evaluation for function
 - Can account for aerostatic effects if needed
- Linear system
 - complex variable, block Jacobi – BILU preconditioner
- Mode tracking
 - Cheap solution of nonlinear eigenvalue problems
 - small steps can be taken
- Highly parallel
 - Each mode can be tracked independently

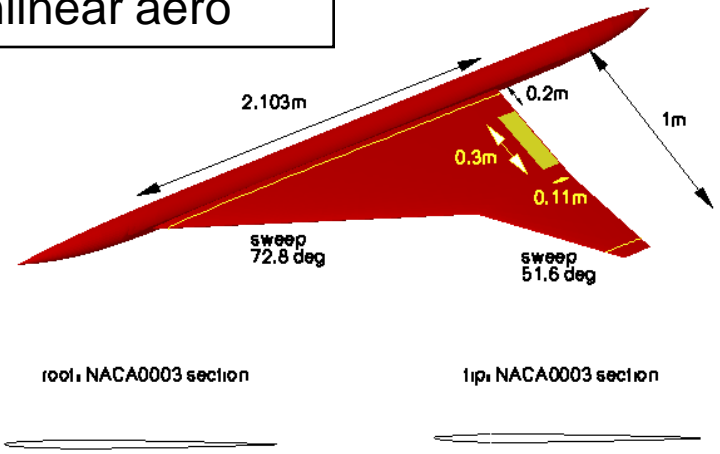
SST control surface buzz

- driven by nonlinear aero



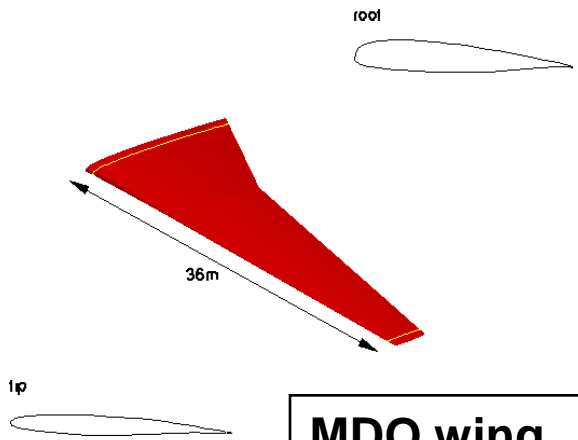
Golland wing

- very flexible – test for series



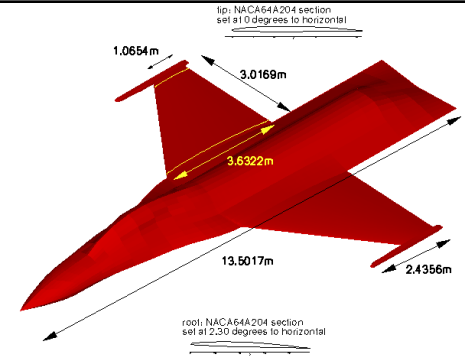
Generic Fighter

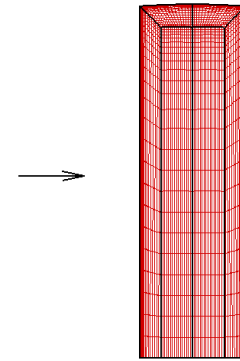
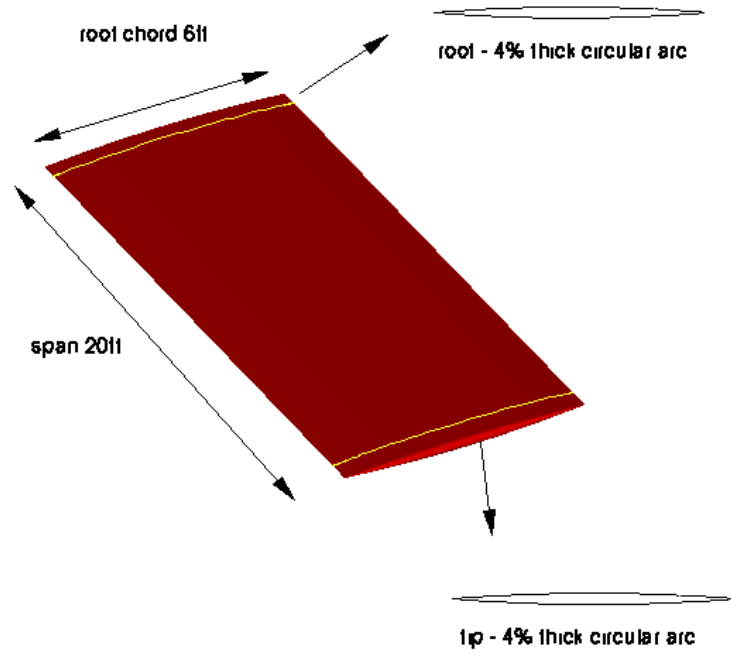
- realistic sized problem



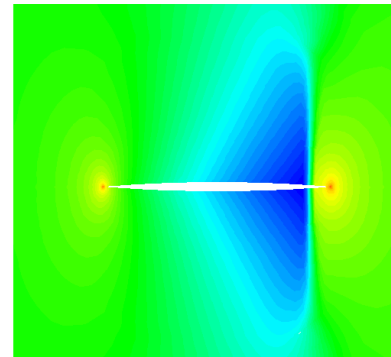
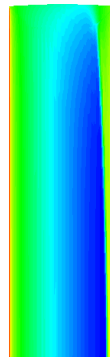
MDO wing

- realistic modes

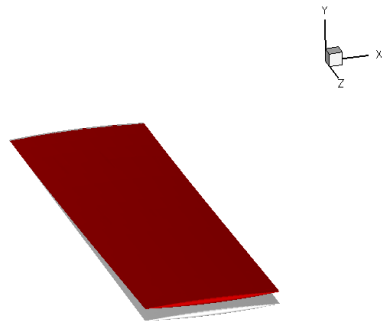




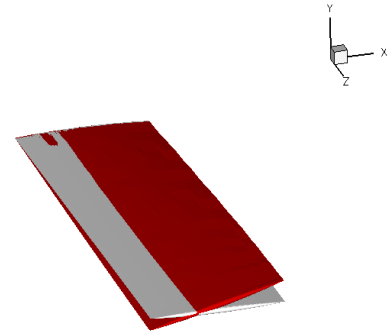
236k points



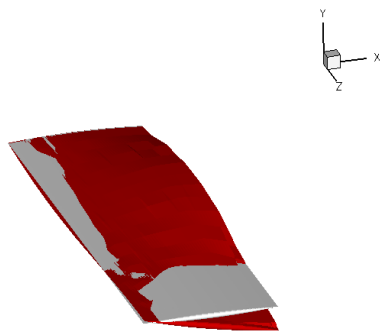
Mach 0.92



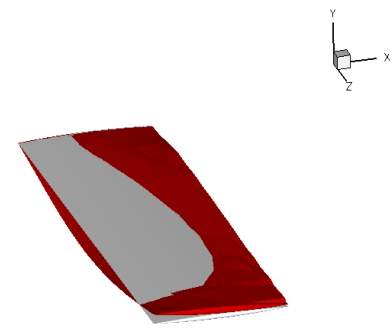
1.72 Hz



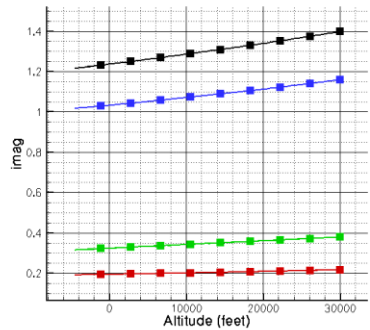
3.05 Hz



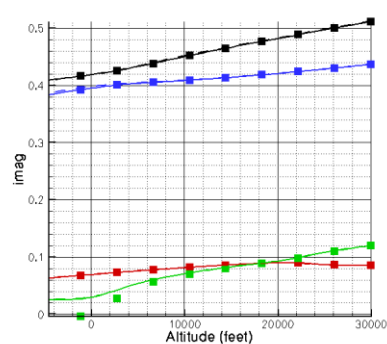
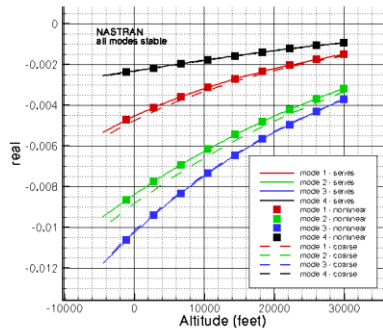
9.18 Hz



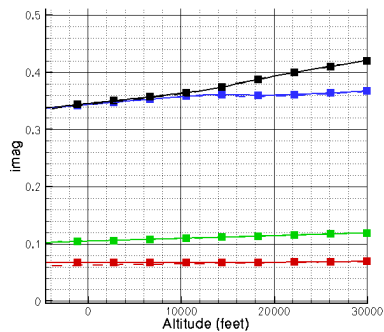
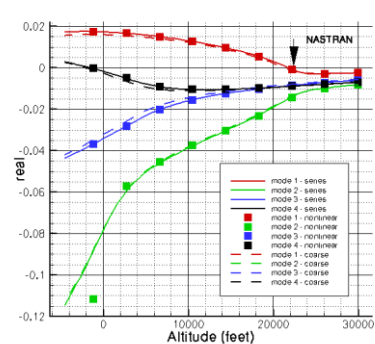
11.10 Hz



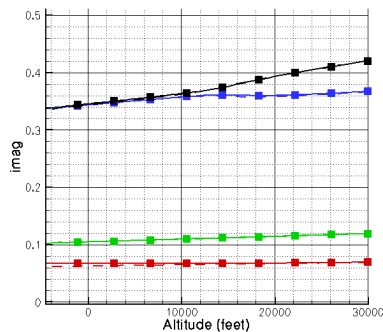
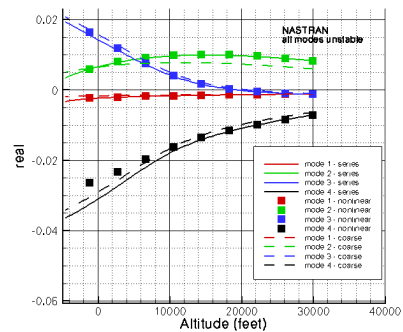
Mach 0.30



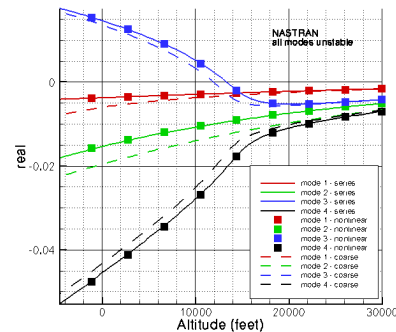
Mach 0.80

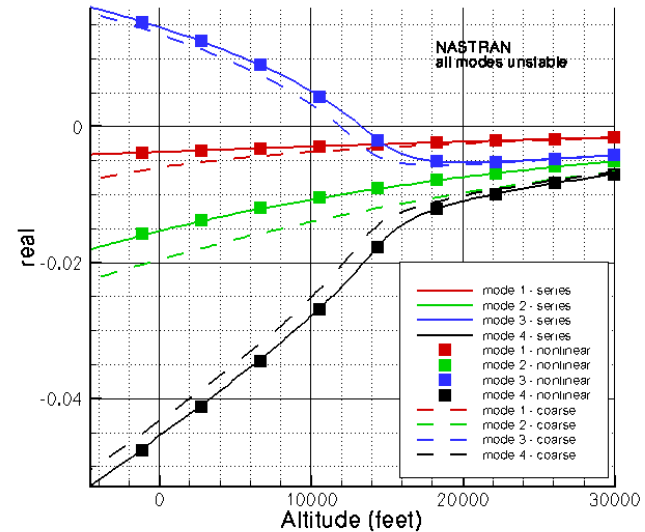
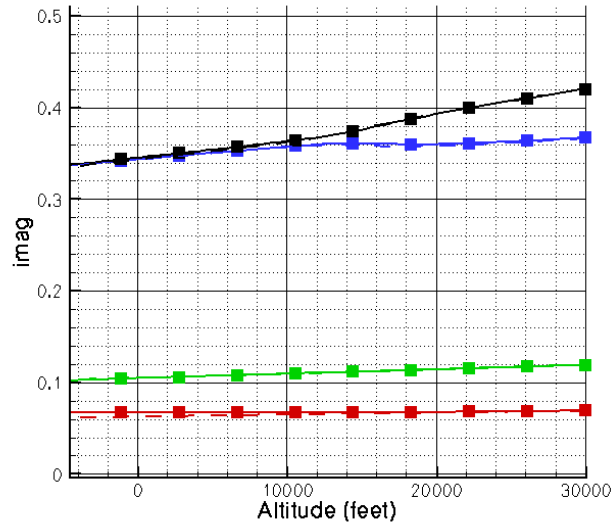


Mach 0.92



Mach 0.97

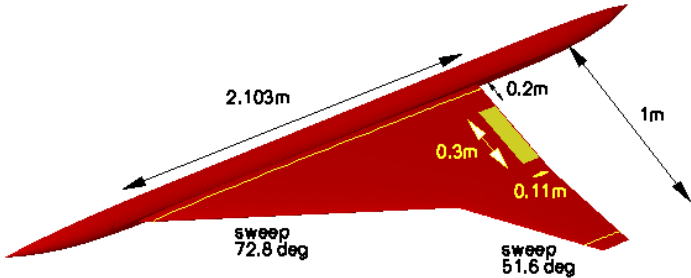




8 processors

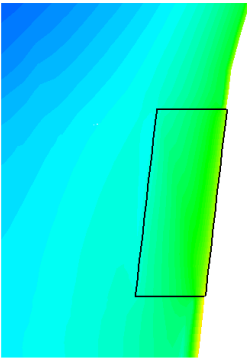
- Steady state in 11 minutes
- 4 modes – generate S - 134 minutes
- Full solution (8) - 202 minutes
- series and full – identical results
- Total cost series method **-13.5 steady state solves**

234k points

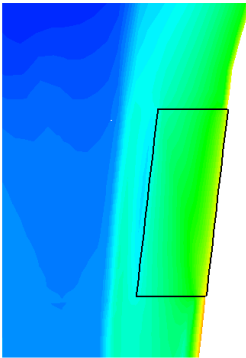


root, NACA0003 section

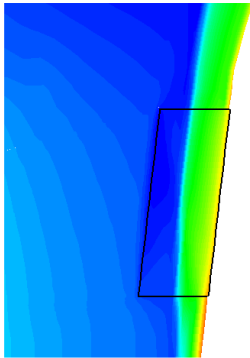
tip, NACA0003 section



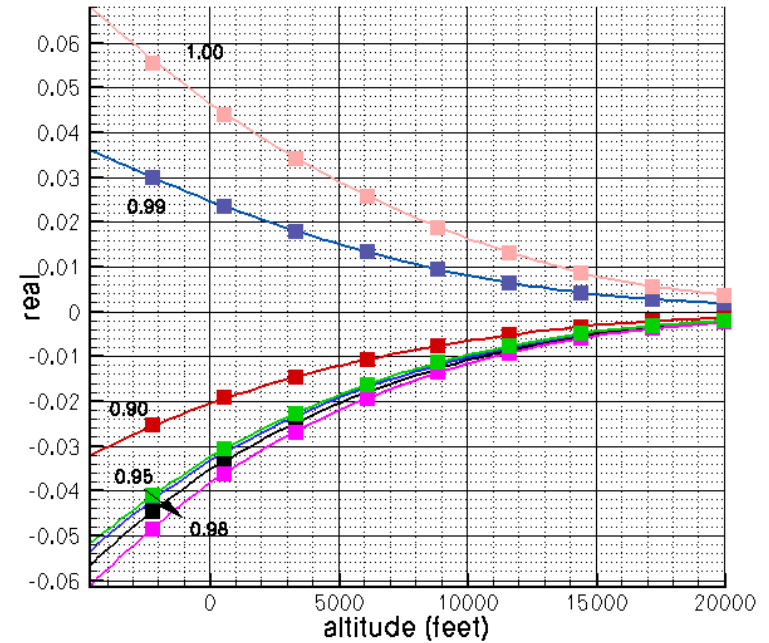
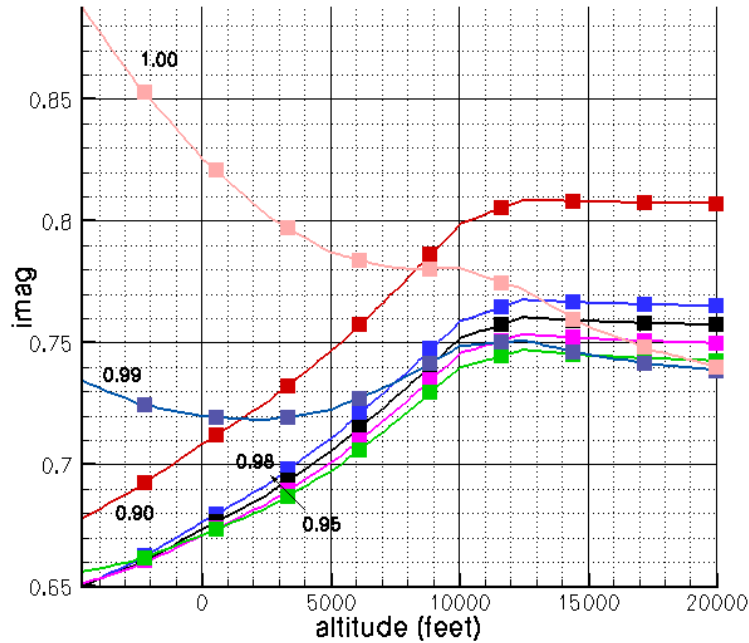
Mach 0.90



Mach 0.96

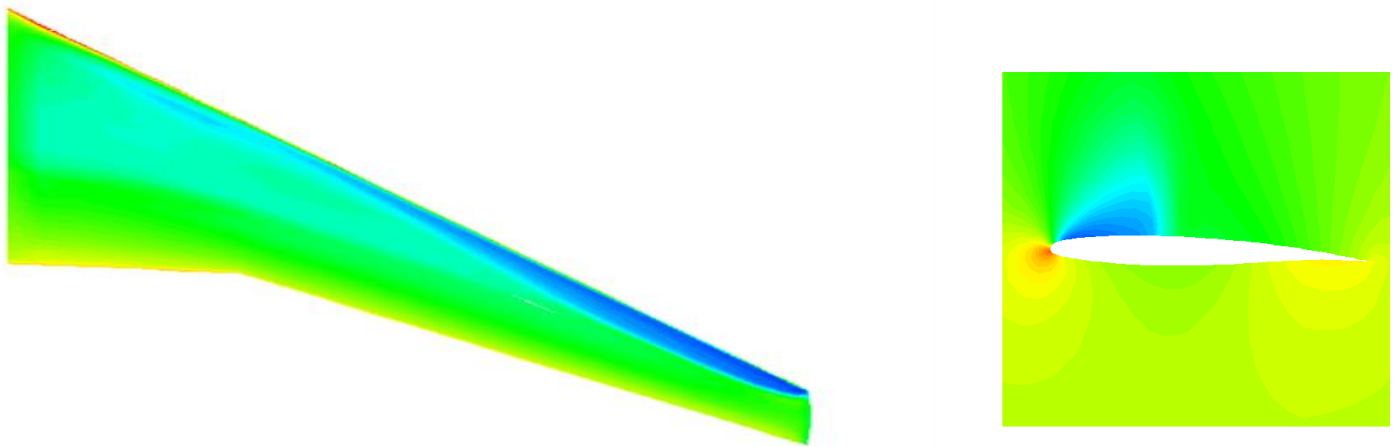
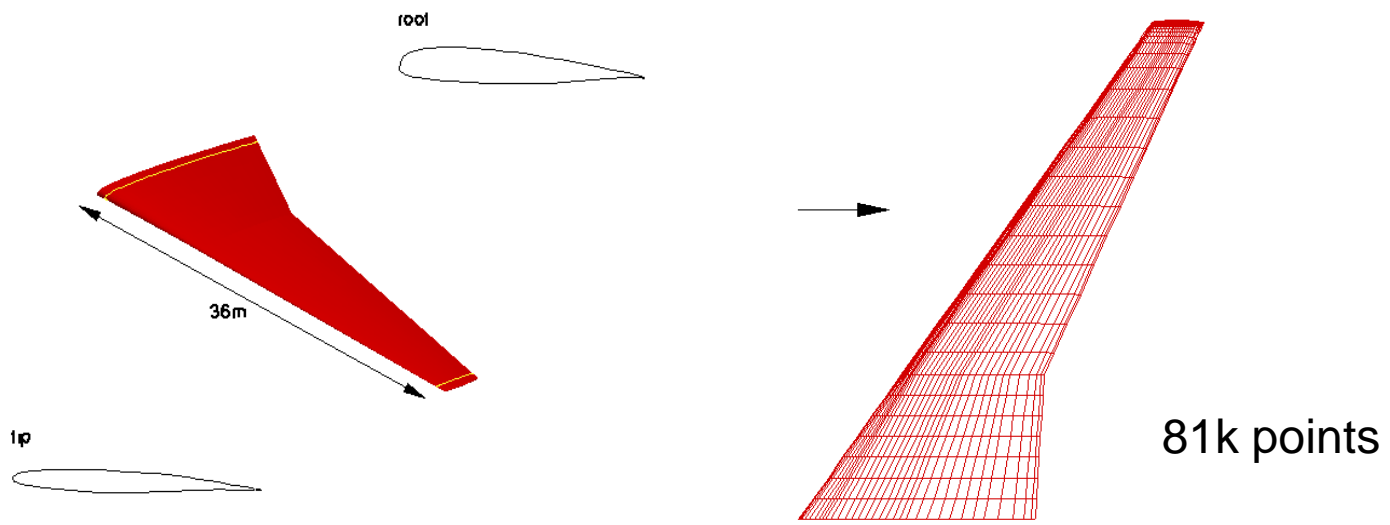


Mach 0.99

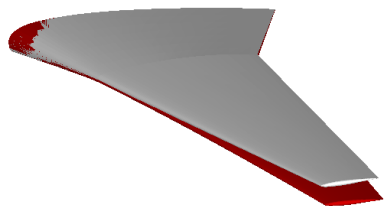


8 processors

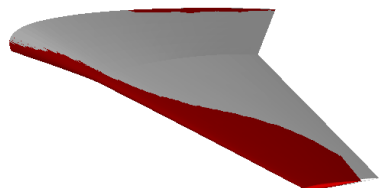
- Per Mach number
 - Steady state in 14 minutes
 - Generate S matrix – 9 minutes
 - Full function evaluation (8) – 49 minutes (23 nonlinear steps)
- series and full solutions identical
- Total cost – series method for 6 Mach nos – **11.5 times steady state**



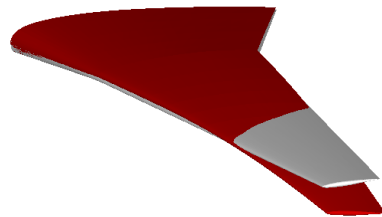
Mach 0.85



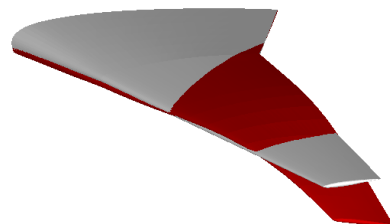
0.88 Hz



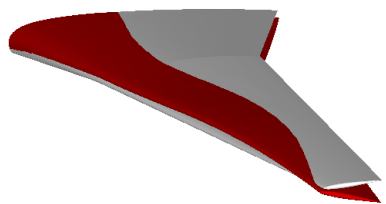
1.79 Hz



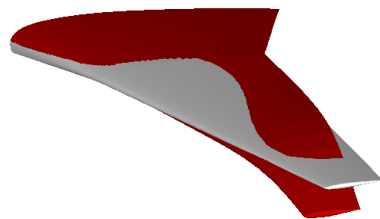
2.23 Hz



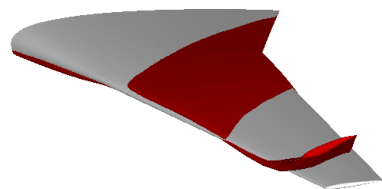
3.69 Hz



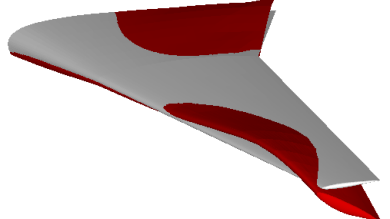
4.10 Hz



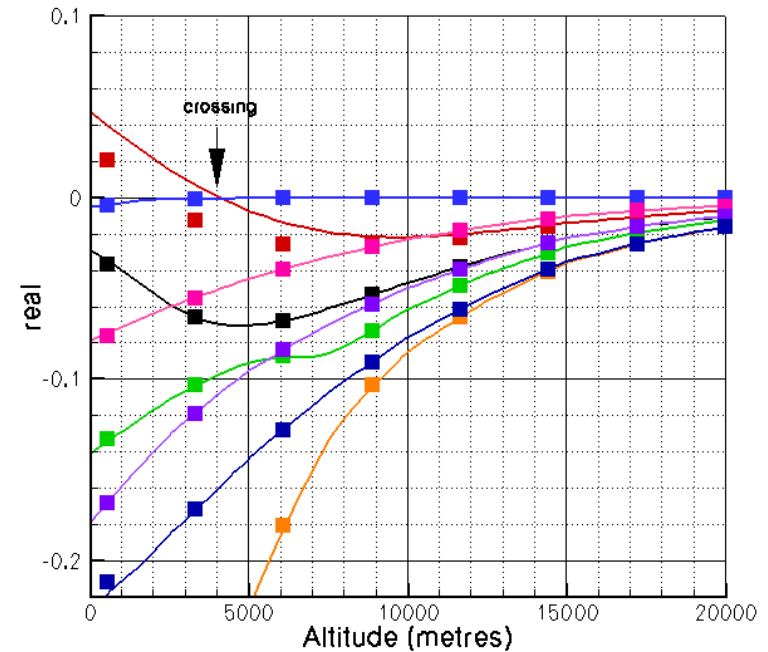
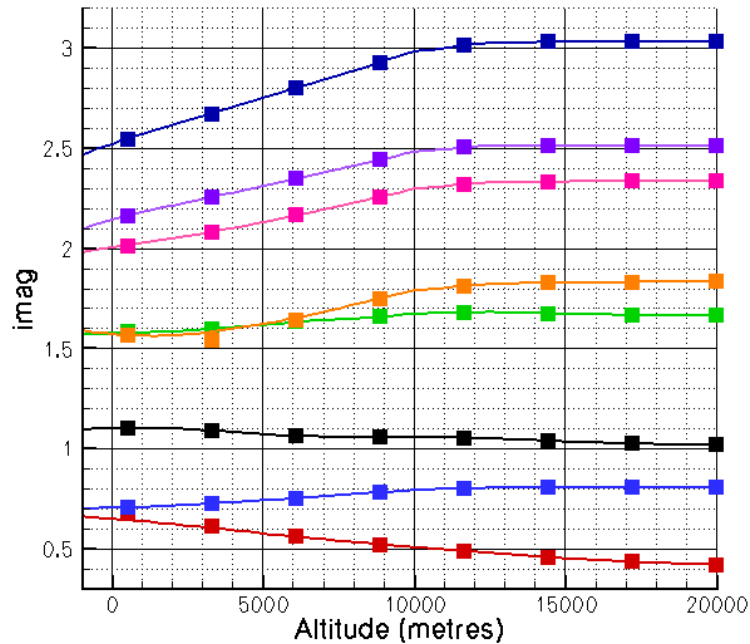
5.21 Hz



5.59 Hz

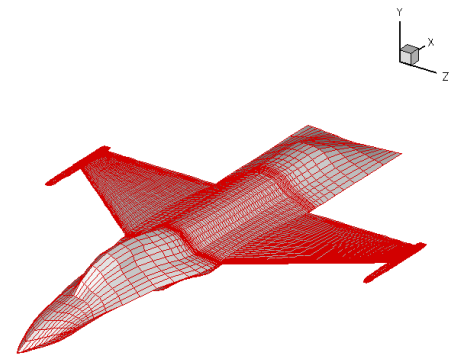
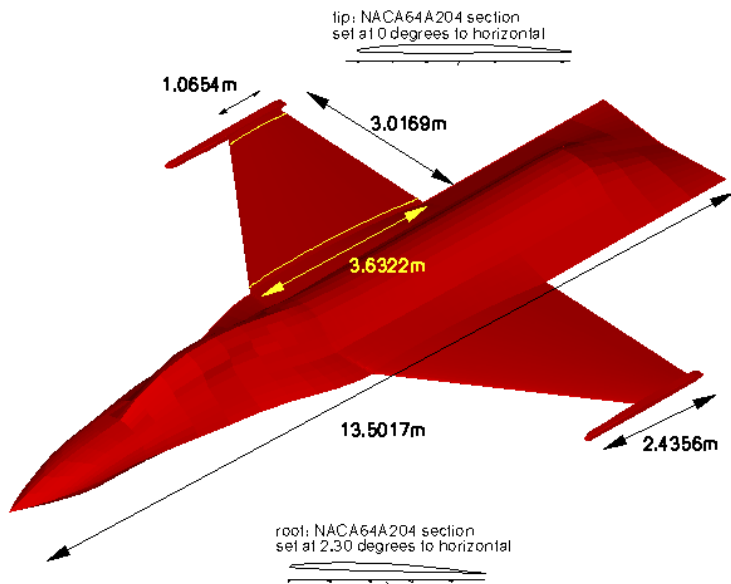


6.76 Hz

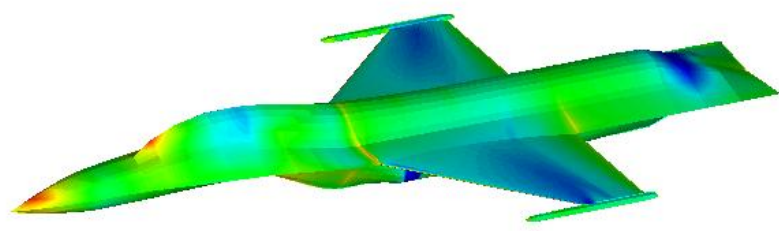
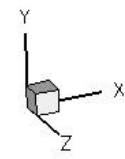


8 processors

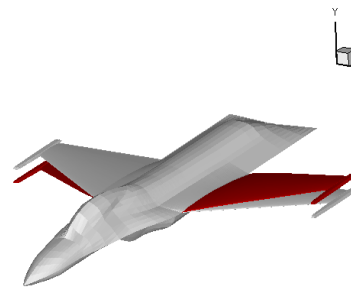
- Steady state in 22 minutes
- for 8 modes – generate S – total time 95 minutes
- Full function evaluation - each mode took 72 minutes
- series and full solutions identical
- Total cost – series method for 8 modes - **5 times steady state**



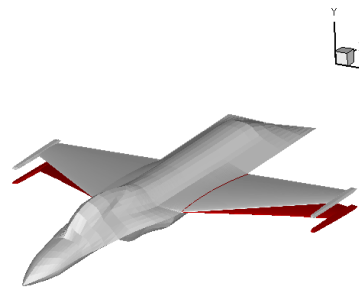
890k points



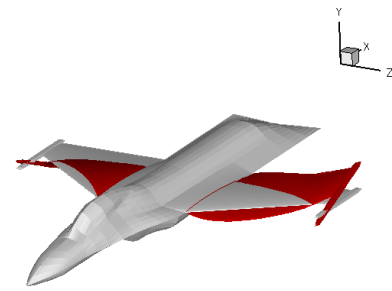
Mach 0.85



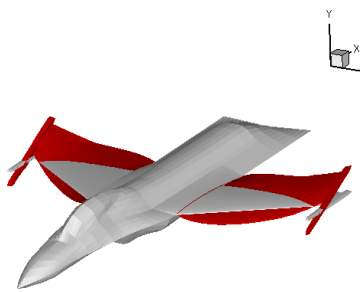
1.72 Hz



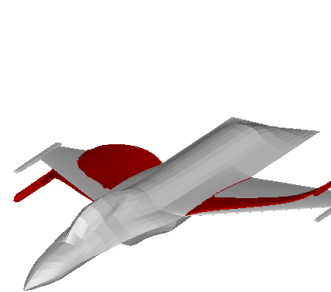
2.52 Hz



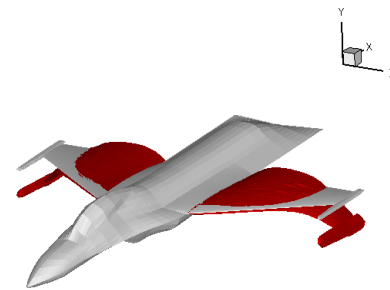
7.61 Hz



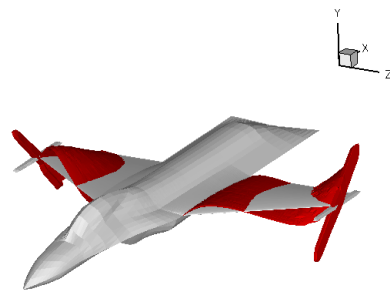
8.50 Hz



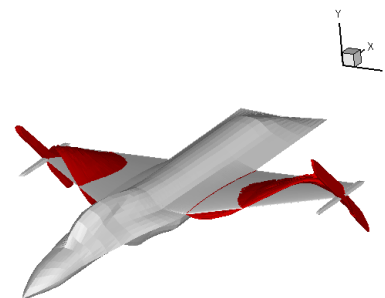
10.22 Hz



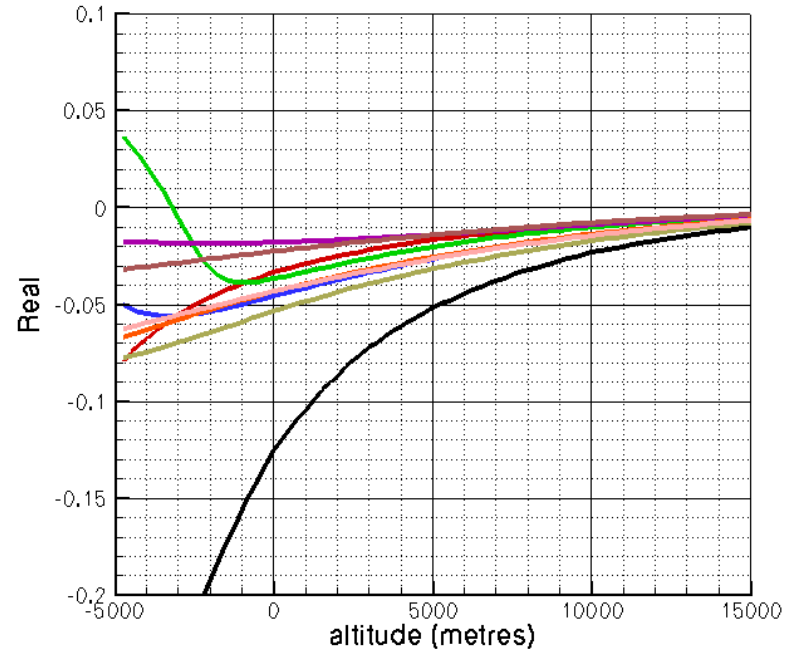
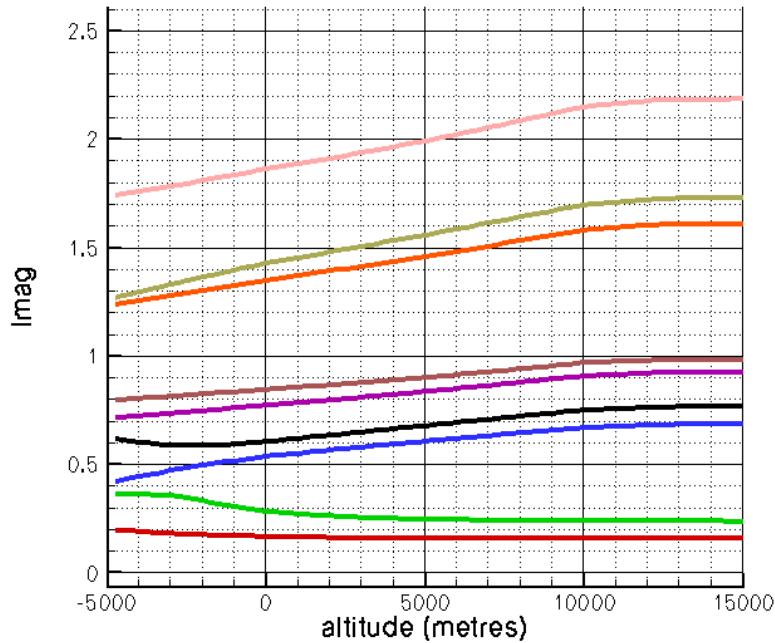
10.80 Hz



17.76 Hz



19.10 Hz



Mach 0.85

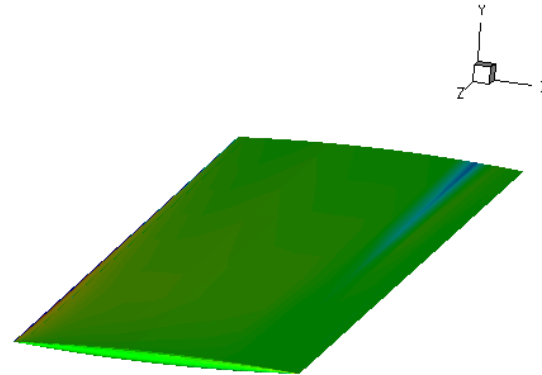
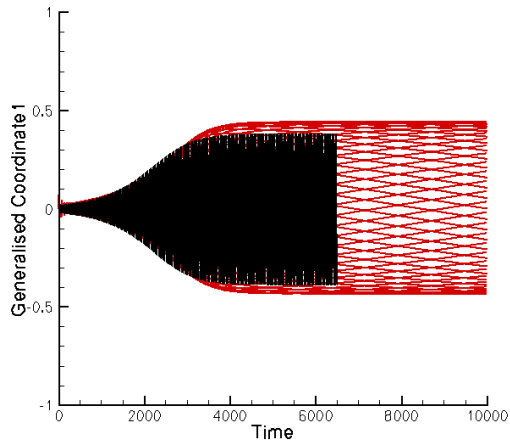
32 processors

- Steady state in 15 minutes
- For each mode – generate S - 45 minutes
- Total cost - series method for 10 modes – **30 times steady state**

Conclusions

- New method proposed
 - mode tracking (robust for all tests)
 - parallel linear solution
 - **100-220 iterations for all cases shown**
- Application to 4 contrasting test cases
 - Series solution works well in all cases
 - Costs per Mach number
 - **5-30 times steady state cost**
 - Information about mechanisms provided
 - Detailed and familiar

Future Work



- ROM to predict LCO
 - Based on critical eigenvector
- Demonstrated for Goland wing
- Can now develop a parallel version of this approach
 - Application to aircraft LCO